

使用部材 □- 476 x 476 x 13.0 x 13.0 $Z_x = 3617.0 \text{ cm}^3$ $I_x = 86087 \text{ cm}^4$ $A = 240.80 \text{ cm}^2$
 角形鋼 $Z_y = 3617.0 \text{ cm}^3$ $I_y = 86087 \text{ cm}^4$
 $Z_{px} = 4181.0 \text{ cm}^3$ $* i_y = \text{---}$ $k_c = 1.00$
 $Z_{py} = 4181.0 \text{ cm}^3$
 ○ 2C5 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{kx} = 396.00 \text{ cm}$
 $L_{ky} = 396.00 \text{ cm}$
 $(M_2 / M_1) = 1.000$

部材種別 = 鉛直軸力 = 268.80 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b: M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b: (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b] / (1.29 - p \lambda b)) \times M_p$ $\lambda b > e \lambda b: M_p / \lambda b^2 =$

$M_e = C \times Z \times \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f)$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / * i_y)^2$ $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1)$ $\lambda b = \sqrt{M_p / M_e} =$

$M_{LB} = (1 - N / N_{LB}) \times Z \times \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z \times \min \{ \text{----} \}$

※、上記結果によらず $M_b = M_p =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 0.234$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pc} = M_b$ $N / N_y > 0.15 : M_{pc} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.043$

$M_{pc} = 1080.79 =$

使用部材 □- 482 x 482 x 16.0 x 16.0 角形鋼
 ○ 2C6、2C7

$Z_x = 4484.0 \text{ cm}^3$ $I_x = 108068 \text{ cm}^4$ $A = 298.20 \text{ cm}^2$
 $Z_y = 4484.0 \text{ cm}^3$ $I_y = 108068 \text{ cm}^4$
 $Z_{px} = 5214.0 \text{ cm}^3$ $* i_y =$ $k_c = 1.00$
 $Z_{py} = 5214.0 \text{ cm}^3$
 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{kx} = 396.00 \text{ cm}$
 $L_{ky} = 396.00 \text{ cm}$
 $(M_2 / M_1) = 1.000$

部材種別 = 鉛直軸力 = 1103.10 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b: M_{FTB} = M_p \quad e \lambda b \geq \lambda b > p \lambda b: (1 - 0.4 \times [(\sqrt{M_p/M_e}) - p \lambda b] / (1.29 - p \lambda b)) \times M_p$ $\lambda b > e \lambda b: M_p / \lambda b^2 =$

$M_e = C \times Z_x \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f)$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / * i_y)^2$ $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1)$ $\lambda b = \sqrt{M_p/M_e} =$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \min \{$ $\}$

※、上記結果によらず $M_b = M_p =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 0.232$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k c^2 \times L_{by}^2) =$

※、 $N_c =$

$N/N_y \leq 0.15 : M_{pc} = M_b$ $N/N_y > 0.15 : M_{pc} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.143$

$M_{pc} = 1347.82 =$

使用部材 □- 482 x 482 x 16.0 x 16.0 角形鋼
 ○ 2C10、2C11 (SM50A)

$Z_x = 4484.0 \text{ cm}^3$ $I_x = 108068 \text{ cm}^4$ $A = 298.20 \text{ cm}^2$
 $Z_y = 4484.0 \text{ cm}^3$ $I_y = 108068 \text{ cm}^4$
 $Z_{px} = 5214.0 \text{ cm}^3$ $* i_y = \text{---}$ $k_c = 1.00$
 $Z_{py} = 5214.0 \text{ cm}^3$
 $F = 325 \text{ N/mm}^2$ $F_u = 490 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{kx} = 420.00 \text{ cm}$
 $L_{ky} = 420.00 \text{ cm}$
 $(M_2 / M_1) = 1.000$

部材種別 = 鉛直軸力 = 1622.40 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b : M_{FTB} = M_p - e \lambda b \geq \lambda b > p \lambda b : (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b] / (1.29 - p \lambda b)) \times M_p$ $\lambda b > e \lambda b : M_p / \lambda b^2 =$

$M_e = C \times Z_x \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f)$ ----

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / * i_y)^2$ ---- $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1)$ ---- $\lambda b = \sqrt{M_p / M_e} =$ ----

$M_{LB} = (1 - N / N_{LB}) \times Z_x \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \min \{ \text{----} \text{----} \}$

※、上記結果によらず $M_b = M_p =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 0.290$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pc} = M_b$ $N / N_y > 0.15 : M_{pc} = 1.18 \times M_b \times (1 - N / N_y)$ $N / N_y = 0.152$
 $1.18 \times 1864.01 \times (1 - (1622.4 / 10047.74))$ 1844.38

$M_{pb} = 1844.37 =$

使用部材 H- 350 x 350 x 12.0 x 19.0 $Z_x = 2280.0 \text{ cm}^3$ $I_x = 39800 \text{ cm}^4$ $A = 171.90 \text{ cm}^2$
 H形弱軸 $Z_y = 776.0 \text{ cm}^3$ $I_y = 13600 \text{ cm}^4$
 $Z_{px} = 2520.0 \text{ cm}^3$ * $i_y = 9.71 \text{ cm}$ $k_c = 1.00$
 $Z_{py} = 1180.0 \text{ cm}^3$
 ○ 2C18 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{kx} = 445.00 \text{ cm}$
 $L_{ky} = 445.00 \text{ cm}$
 $(M_2 / M_1) = 0.000$

部材種別 = FA 鉛直軸力 = 242.50 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$ 305.03 KNm

$M_{FTB} = \rho \lambda b \geq \lambda b : M_{FTB} = M_p - e \lambda b \geq \lambda b > \rho \lambda b : (1 - 0.4 \times [\{ (\sqrt{M_p / M_e}) - \rho \lambda b \} / (1.29 - \rho \lambda b)]) \times M_p$ $\lambda b > e \lambda b : M_p / \lambda b^2 =$ 305.03 KNm

$M_e = C \times Z \times \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$ 7375.99 KNm

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$ $\rightarrow C = 1.75$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 58.28 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 175.43 \text{ KN/cm}^2$ $e \lambda b = 1.29$

$\rho \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.600$ $\lambda b = \sqrt{M_p / M_e} = 0.20$

$M_{LB} = (1 - N / N_{LB}) \times Z \times \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z \times \min \{ 269.83, 300.87 \} =$ ---- ←← FA、FBは省略
 $N_{LB} = N_y / (0.60 + 1.60 \times F_y / E \times (b / t_f)^2 + 0.15 \times F_w / E \times (d / t_w)^2) = 3290.67 \text{ KN}$

※、上記結果により $M_b =$ 305.03 KNm

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 0.559$

$N_y = F \times A =$ 4443.62 KN

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) =$ 41656.43 KN

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) =$ 14234.36 KN

※、 $N_c =$ 4116.09 KN

$N / N_y \leq 0.4 : M_{pc} = M_b$ $N / N_y > 0.4 : M_{pc} = 1.19 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.055$

$M_{pc} = 305.03 =$ 305.03 KNm

使用部材 □- 482 x 482 x 16.0 x 16.0 角形鋼
 ○ PHC6、PHC7

$Z_x = 4484.0 \text{ cm}^3$ $I_x = 108068 \text{ cm}^4$ $A = 298.20 \text{ cm}^2$
 $Z_y = 4484.0 \text{ cm}^3$ $I_y = 108068 \text{ cm}^4$
 $Z_{px} = 5214.0 \text{ cm}^3$ $* i_y = \text{---}$ $k_c = 1.00$
 $Z_{py} = 5214.0 \text{ cm}^3$
 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{kx} = 456.00 \text{ cm}$
 $L_{ky} = 456.00 \text{ cm}$
 $(M_2 / M_1) = 1.000$

部材種別 = 鉛直軸力 = 480.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b : M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b : (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b] / (1.29 - p \lambda b)) \times M_p$ $\lambda b > e \lambda b : M_p / \lambda b^2 =$

$M_e = C \times Z_x \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f)$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / * i_y)^2$ $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1)$ $\lambda b = \sqrt{M_p / M_e} =$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \min \{ \text{----} \text{----} \}$

※、上記結果によらず $M_b = M_p =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 0.268$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pc} = M_b$ $N / N_y > 0.15 : M_{pc} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.062$

$M_{pc} = 1347.82 =$

使用部材 H- 350 x 350 x 12.0 x 19.0 $Z_x = 2280.0 \text{ cm}^3$ $I_x = 39800 \text{ cm}^4$ $A = 171.90 \text{ cm}^2$
 II形強軸 $Z_y = 776.0 \text{ cm}^3$ $I_y = 13600 \text{ cm}^4$
 $Z_{px} = 2730.0 \text{ cm}^3$ * $i_y = 9.71 \text{ cm}$ $k_c = 1.00$
 $Z_{py} = 1240.0 \text{ cm}^3$
 ○ PHC18 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{kx} = 448.00 \text{ cm}$
 $L_{ky} = 448.00 \text{ cm}$
 $(M_2 / M_1) = 1.000$

部材種別 = FA 鉛直軸力 = 182.50 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$ 705.71 KNm

$M_{FTB} = p \lambda b \geq \lambda b: M_{FTB} = M_p \quad e \lambda b \geq \lambda b > p \lambda b: (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b] / (1.29 - p \lambda b)) \times M_p$
 $\lambda b > e \lambda b: M_p / \lambda b^2 =$ 705.71 KNm

$M_e = C \times Z \times \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$ 9571.19 KNm

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30 \rightarrow C = 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 57.89 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 173.09 \text{ KN/cm}^2 \quad e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.900 \quad \lambda b = \sqrt{M_p / M_e} = 0.27$

$M_{LB} = (1 - N / N_{LB}) \times Z \times \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z \times \min \{ 269.83, 300.87 \} =$ ----- ←← FA、FBは省略
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 3290.67 \text{ KN}$

※、上記結果により $M_b =$ 705.71 KNm

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 0.562$

$N_y = F \times A =$ 4443.62 KN

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) =$ 41100.40 KN

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) =$ 14044.36 KN

※、 $N_c =$ 4111.78 KN

$N / N_y \leq 0.15 : M_{pc} = M_b \quad N / N_y > 0.15 : M_{pc} = 1.18 \times M_b \times (1 - N / N_y) \quad N / N_y = 0.041$

$M_{pc} = 705.71 =$ 705.71 KNm

4) 梁の終局耐力の算定 防災協会仕様

使用部材 H- 700 x 300 x 13.0 x 24.0 $Z_x = 5640.0 \text{ cm}^3$ $I_x = 197000 \text{ cm}^4$ $A = 231.50 \text{ cm}^2$
 H形強軸 $I_y = 10800 \text{ cm}^4$
 $Z_p = 6340.0 \text{ cm}^3$ * $i_y = 7.95 \text{ cm}$ $k_c = 1.00$
 ○ 2G1 端部 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{bx} = 1200.00 \text{ cm}$
 $L_{by} = 1200.00 \text{ cm}$
 $(M_2 / M_1) = 1.000$

部材種別 = 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b : M_{FTB} = M_p - e \lambda b \geq \lambda b > p \lambda b : (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b]) / (1.29 - p \lambda b) \times M_p$ $\lambda b > e \lambda b : M_p / \lambda b^2 =$

$M_e = C \times Z_x \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$ →→ $C = 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 11.70 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / * i_y)^2 = 16.17 \text{ KN/cm}^2$ $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.900$ $\lambda b = \sqrt{M_p / M_e} = 0.80$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \min \{ 294.44, 276.38 \} =$ ←← FA、FBは省略
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 4379.44 \text{ KN}$

※、上記結果により $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 1.962$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b$ $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.000$

$M_{pb} = 1638.89 =$

※、他の部位の詳細計算は省略して後ページに結果表を作成した。(他の部位の詳細計算は別紙とした。)

使用部材 H- 692 x 300 x 13.0 x 20.0 $Z_x = 4870.0 \text{ cm}^3$ $I_x = 168000 \text{ cm}^4$ $A = 207.50 \text{ cm}^2$
H形強軸 $Z_p = 5500.0 \text{ cm}^3$ $I_y = 9020 \text{ cm}^4$ $* i_y = 7.81 \text{ cm}$ $k_c = 1.00$
○ 2G1 中央 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{bx} = 1200.00 \text{ cm}$
 $L_{by} = 1200.00 \text{ cm}$
 $(M_2 / M_1) = 1.000$

部材種別 = 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b : M_{FTB} = M_p - e \lambda b \geq \lambda b > p \lambda b : (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b]) / (1.29 - p \lambda b) \times M_p$ $\lambda b > e \lambda b : M_p / \lambda b^2 =$

$M_e = C \times Z_x \times \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$ $\rightarrow \rightarrow C = 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 9.86 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / * i_y)^2 = 15.61 \text{ KN/cm}^2$ $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.900$ $\lambda b = \sqrt{M_p / M_e} = 0.83$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \times \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \times \min \{ 284.05, 276.38 \} =$ ←← FA、FBは省略
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 3627.96 \text{ KN}$

※、上記結果により $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 2.033$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b$ $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.000$

$M_{pb} = 1421.75 =$

使用部材 H- 692 x 300 x 13.0 x 20.0 $Z_x = 4870.0 \text{ cm}^3$ $I_x = 168000 \text{ cm}^4$ $A = 207.50 \text{ cm}^2$
 H形強軸 $I_y = 9020 \text{ cm}^4$
 $Z_p = 5500.0 \text{ cm}^3$ * $i_y = 7.81 \text{ cm}$ $k_c = 1.00$
 ○ 2G2 端部 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{bx} = 1000.00 \text{ cm}$
 $L_{by} = 250.00 \text{ cm}$
 $(M_2 / M_1) = -0.500$

部材種別 = 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b : M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b : (1 - 0.4 \times [(\sqrt{M_p/M_e}) - p \lambda b]) / (1.29 - p \lambda b) \times M_p$ $\lambda b > e \lambda b : M_p / \lambda b^2 =$

$M_e = C \times Z_x \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$ →→→ $C = 1.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 47.34 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 359.60 \text{ KN/cm}^2$ $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.450$ $\lambda b = \sqrt{M_p/M_e} = 0.25$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \times \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \times \min \{ 284.05, 276.38 \} =$ ←← FA、FBは省略
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 3627.96 \text{ KN}$

※、上記結果により $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 0.423$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b$ $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.000$

$M_{pb} = 1421.75 =$

使用部材 H- 692 x 300 x 13.0 x 20.0 $Z_x = 4870.0 \text{ cm}^3$ $I_x = 168000 \text{ cm}^4$ $A = 207.50 \text{ cm}^2$
H形強軸 $Z_p = 5500.0 \text{ cm}^3$ $I_y = 9020 \text{ cm}^4$ $kc = 1.00$
○ 2G2 中央 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{bx} = 1000.00 \text{ cm}$
 $L_{by} = 250.00 \text{ cm}$
 $(M_2 / M_1) = 0.000$

部材種別 = FA 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p = 1421.75 \text{ KNm}$

$M_{FTB} = p \lambda b \geq \lambda b: M_{FTB} = M_p \quad e \lambda b \geq \lambda b > p \lambda b: (1 - 0.4 \times [(\sqrt{M_p/M_e}) - p \lambda b]) / (1.29 - p \lambda b) \times M_p$
 $\lambda b > e \lambda b: M_p / \lambda b^2 = 1421.75 \text{ KNm}$

$M_e = C \times Z_x \times \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)} = 30911.27 \text{ KNm}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30 \rightarrow C = 1.75$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 47.34 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 359.60 \text{ KN/cm}^2 \quad e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.600 \quad \lambda b = \sqrt{M_p/M_e} = 0.21$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \times \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \times \min \{ 284.05, 276.38 \} = \text{-----}$ ←← FA、FBは省略
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 3627.96 \text{ KN}$

※、上記結果により $M_b = 1421.75 \text{ KNm}$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 0.423$

$N_y = F \times A = 5363.88 \text{ KN}$

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) = 34819.96 \text{ KN}$

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) = 29912.01 \text{ KN}$

※、 $N_c = 4813.04 \text{ KN}$

$N / N_y \leq 0.15 : M_{pb} = M_b \quad N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c) \quad N / N_y = 0.000$

$M_{pb} = 1421.75 = 1421.75 \text{ KNm}$

使用部材 BH- 1300 x 450 x 16.0 x 32.0 $Z_x = 21686.8 \text{ cm}^3$ $I_x = 1409643 \text{ cm}^4$ $A = 485.76 \text{ cm}^2$
H形強軸 $Z_p = 24528.2 \text{ cm}^3$ $I_y = 48642 \text{ cm}^4$ $* i_y = 12.99 \text{ cm}$ $k_c = 1.00$

○ 2G3 端部 (SM50A)

$F = 325 \text{ N/mm}^2$ $F_u = 490 \text{ N/mm}^2$
強度割増 = 1.1 倍 $L_{bx} = 1000.00 \text{ cm}$
 $L_{by} = 1000.00 \text{ cm}$
 $(M_2 / M_1) = 1.000$

部材種別 = 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b: M_{FTB} = M_p - e \lambda b \geq \lambda b > p \lambda b: (1 - 0.4 \times [(\sqrt{M_p/M_e}) - p \lambda b] / (1.29 - p \lambda b)) \times M_p$ $\lambda b > e \lambda b: M_p / \lambda b^2 =$

$M_e = C \times Z_x \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$ $\rightarrow C = 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 15.12 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / * i_y)^2 = 62.19 \text{ KN/cm}^2$ $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.900$ $\lambda b = \sqrt{M_p/M_e} = 0.52$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \min \{ 383.99, 325.18 \} =$
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) =$

※、上記結果により $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 1.312$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k c^2 \times L_{by}^2) =$

※、 $N_c =$

$N/N_y \leq 0.15 : M_{pb} = M_b$ $N/N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.000$

$M_{pb} = 7052.21 =$

使用部材 BH- 1300 x 300 x 16.0 x 32.0 $Z_x = 15749.0 \text{ cm}^3$ $I_x = 1023684 \text{ cm}^4$ $A = 389.76 \text{ cm}^2$
H形強軸 $Z_p = 18441.8 \text{ cm}^3$ * $i_y = 8.66 \text{ cm}$ $k_c = 1.00$
○ 2G3 中央 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{bx} = 1000.00 \text{ cm}$
 $L_{by} = 1000.00 \text{ cm}$
 $(M_2 / M_1) = 1.000$

部材種別 = 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b : M_{FTB} = M_p - e \lambda b \geq \lambda b > p \lambda b : (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b] / (1.29 - p \lambda b)) \times M_p$ $\lambda b > e \lambda b : M_p / \lambda b^2 =$

$M_e = C \times Z_x \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30 \rightarrow C = 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 10.08 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 27.66 \text{ KN/cm}^2$ $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.900$ $\lambda b = \sqrt{M_p / M_e} = 0.67$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \min \{ 307.43, 248.92 \} =$

$N_{LB} = N_y / (0.60 + 1.60 \times F_y / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 5400.90 \text{ KN}$

※、上記結果により $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 1.835$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b$ $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_y)$ $N / N_y = 0.000$

$M_{pb} = 3920.16 =$

使用部材 BH- 700 x 450 x 16.0 x 36.0 $Z_x = 11157.1 \text{ cm}^3$ $I_x = 390499 \text{ cm}^4$ $A = 424.48 \text{ cm}^2$
H形強軸 $I_y = 51696 \text{ cm}^4$
 $Z_p = 12424.8 \text{ cm}^3$ * $i_y = 12.99 \text{ cm}$ $k_c = 1.00$
○ 2G4 端部 (SM50A) $F = 325 \text{ N/mm}^2$ $F_u = 490 \text{ N/mm}^2$
強度割増 = 1.1 倍 $L_{bx} = 1000.00 \text{ cm}$
 $L_{by} = 250.00 \text{ cm}$
 $(M_2 / M_1) = -0.500$

部材種別 = 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b: M_{FTB} = M_p - e \lambda b \geq \lambda b > p \lambda b: (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b] / (1.29 - p \lambda b)) \times M_p$ $\lambda b > e \lambda b: M_p / \lambda b^2 =$

$M_e = C \times Z_x \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$ $\rightarrow C = 1.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 126.36 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 994.96 \text{ KN/cm}^2$ $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.450$ $\lambda b = \sqrt{M_p / M_e} = 0.17$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \min \{ 394.56, 387.83 \} =$ $\leftarrow \leftarrow$ FA、FBは省略
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 10602.80 \text{ KN}$

※、上記結果により $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 0.433$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b$ $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.000$

$M_{pb} = 4441.85 =$

使用部材 BH- 700 x 400 x 16.0 x 36.0 $Z_x = 10022.3 \text{ cm}^3$ $I_x = 350779 \text{ cm}^4$ $A = 388.48 \text{ cm}^2$
H形強軸 $Z_p = 11229.6 \text{ cm}^3$ * $i_y = 11.55 \text{ cm}$ $k_c = 1.00$
○ 2G4 中央 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{bx} = 1000.00 \text{ cm}$
 $L_{by} = 250.00 \text{ cm}$
 $(M_2 / M_1) = 0.000$

部材種別 = 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b: M_{FTB} = M_p - e \lambda b \geq \lambda b > p \lambda b: (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b]) / (1.29 - p \lambda b) \times M_p$ $\lambda b > e \lambda b: M_p / \lambda b^2 =$

$M_e = C \times Z \times \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$ $\rightarrow C = 1.75$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 112.32 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 786.17 \text{ KN/cm}^2$ $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.600$ $\lambda b = \sqrt{M_p / M_e} = 0.14$

$M_{LB} = (1 - N / N_{LB}) \times Z \times \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z \times \min \{ 300.21, 287.44 \} =$ ←← FA、FBは省略
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 8790.94 \text{ KN}$

※、上記結果により $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 0.372$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b$ $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.000$

$M_{pb} = 2902.84 =$

使用部材 BH- 1300 x 400 x 16.0 x 32.0 $Z_x = 19707.5 \text{ cm}^3$ $I_x = 1280990 \text{ cm}^4$ $A = 453.76 \text{ cm}^2$
H形強軸 $Z_p = 22499.4 \text{ cm}^3$ $I_y = 34176 \text{ cm}^4$ $k_c = 1.00$
 $* i_y = 11.55 \text{ cm}$

○ 2G5 端部 (SM50A)

$F = 325 \text{ N/mm}^2$ $F_u = 490 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{bx} = 1000.00 \text{ cm}$
 $L_{by} = 500.00 \text{ cm}$
 $(M_2 / M_1) = 0.000$

部材種別 = 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b: M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b: (1 - 0.4 \times [(\sqrt{M_p/M_e}) - p \lambda b]) / (1.29 - p \lambda b)$ $\lambda b > e \lambda b: M_p / \lambda b^2 =$

$M_e = C \times Z_x \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$ $\rightarrow C = 1.75$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 26.88 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / * i_y)^2 = 196.59 \text{ KN/cm}^2$ $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.600$ $\lambda b = \sqrt{M_p/M_e} = 0.34$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \min \{ 394.56, 325.18 \} =$

$N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) =$

※、上記結果により $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 0.757$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b$ $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.000$

$M_{pb} = 6408.58 =$

使用部材 BH- 1300 x 300 x 16.0 x 32.0 $Z_x = 15749.0 \text{ cm}^3$ $I_x = 1023684 \text{ cm}^4$ $A = 389.76 \text{ cm}^2$
H形強軸 $Z_p = 18441.8 \text{ cm}^3$ * $i_y = 8.66 \text{ cm}$ $k_c = 1.00$
○ 2G5 中央 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{bx} = 1000.00 \text{ cm}$
 $L_{by} = 500.00 \text{ cm}$
 $(M_2 / M_1) = 0.000$

部材種別 = 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b: M_{FTB} = M_p - e \lambda b \geq \lambda b > p \lambda b: (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b] / (1.29 - p \lambda b)) \times M_p$ $\lambda b > e \lambda b: M_p / \lambda b^2 =$

$M_e = C \times Z \times \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30 \rightarrow C = 1.75$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 20.16 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 110.64 \text{ KN/cm}^2$ $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.600$ $\lambda b = \sqrt{M_p / M_e} = 0.39$

$M_{LB} = (1 - N / N_{LB}) \times Z \times \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z \times \min \{ 307.43, 248.92 \} =$

$N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 5400.90 \text{ KN}$

※、上記結果により $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$

$\lambda_c = 0.917$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b$ $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.000$

$M_{pb} = 3920.16 =$

使用部材 BH- 1300 x 450 x 16.0 x 32.0 $Z_x = 21686.8 \text{ cm}^3$ $I_x = 1409643 \text{ cm}^4$ $A = 485.76 \text{ cm}^2$
H形強軸 $Z_p = 24528.2 \text{ cm}^3$ $I_y = 48642 \text{ cm}^4$ $* i_y = 12.99 \text{ cm}$ $kc = 1.00$

○ 2G6 端部 (SM50A) $F = 325 \text{ N/mm}^2$ $F_u = 490 \text{ N/mm}^2$
Y0-1

強度割増 = 1.1 倍 $L_{bx} = 1000.00 \text{ cm}$
 $L_{by} = 250.00 \text{ cm}$
 $(M_2 / M_1) = -0.500$

部材種別 = 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b: M_{FTB} = M_p \quad e \lambda b \geq \lambda b > p \lambda b: (1 - 0.4 \times [(\sqrt{M_p/M_e}) - p \lambda b]) / (1.29 - p \lambda b) \times M_p$
 $\lambda b > e \lambda b: M_p / \lambda b^2 =$

$M_e = C \times Z_x \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30 \rightarrow C = 1.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 60.48 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / * i_y)^2 = 995.11 \text{ KN/cm}^2 \quad e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.450 \quad \lambda b = \sqrt{M_p/M_e} = 0.18$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \min \{ 383.99, 325.18 \} =$

$N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 6622.70 \text{ KN}$

※、上記結果により $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 0.328$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k c^2 \times L_{by}^2) =$

※、 $N_c =$

$N/N_y \leq 0.15 : M_{pb} = M_b \quad N/N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c) \quad N / N_y = 0.000$

$M_{pb} = 7052.21 =$

使用部材 BH- 1300 x 350 x 16.0 x 32.0 $Z_x = 17728.3 \text{ cm}^3$ $I_x = 1152337 \text{ cm}^4$ $A = 421.76 \text{ cm}^2$
H形強軸 $I_y = 22909 \text{ cm}^4$
 $Z_p = 20470.6 \text{ cm}^3$ * $i_y = 10.11 \text{ cm}$ $k_c = 1.00$

○ 2G6 中央
Y0-1

$F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{bx} = 1000.00 \text{ cm}$
 $L_{by} = 250.00 \text{ cm}$
 $(M_2 / M_1) = 0.000$

部材種別 =

鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b: M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b: (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b] / (1.29 - p \lambda b)) \times M_p$ $\lambda b > e \lambda b: M_p / \lambda b^2 =$

$M_e = C \times Z_x \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$ $\rightarrow C = 1.75$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 47.04 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 602.16 \text{ KN/cm}^2$ $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.600$ $\lambda b = \sqrt{M_p / M_e} = 0.17$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \min \{ 300.93, 248.92 \} =$

$N_{LB} = N_y / (0.60 + 1.60 \times F_y f / E \times (b / t_f)^2 + 0.15 \times F_y w / E \times (d / t_w)^2) =$

※、上記結果により $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 0.379$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b$ $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.000$

$M_{pb} = 4412.83 =$

使用部材 BH- 1300 x 450 x 16.0 x 32.0 $Z_x = 21686.8 \text{ cm}^3$ $I_x = 1409643 \text{ cm}^4$ $A = 485.76 \text{ cm}^2$
H形強軸 $I_y = 48642 \text{ cm}^4$
 $Z_p = 24528.2 \text{ cm}^3$ * $i_y = 12.99 \text{ cm}$ $k_c = 1.00$

○ 2G6 端部
(SM50A)
Y2-4

$F = 325 \text{ N/mm}^2$ $F_u = 490 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{bx} = 1000.00 \text{ cm}$
 $L_{by} = 500.00 \text{ cm}$
 $(M_2 / M_1) = 0.000$

部材種別 =

鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b: M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b: (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b] /$

$$(1.29 - P \lambda b)) \times M_p \quad \lambda b > e \lambda b: M_p / \lambda b^2 = \boxed{8768.83 \text{ KNm}}$$

$$M_e = C \times Z \times \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)} = \boxed{95111.23 \text{ KNm}}$$

$$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30 \quad \rightarrow \rightarrow C = 1.75$$

$$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 30.24 \text{ KN/cm}^2$$

$$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 248.78 \text{ KN/cm}^2 \quad e \lambda b = 1.29$$

$$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.600 \quad \lambda b = \sqrt{M_p / M_e} = 0.30$$

$$M_{LB} = (1 - N / N_{LB}) \times Z \times \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$$

$$= Z \times \min \{ 383.99, 325.18 \} = \boxed{7052.21 \text{ KNm}}$$

$$N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = \boxed{6622.70 \text{ KN}}$$

$$\text{※、上記結果により } M_b = \boxed{7052.21 \text{ KNm}}$$

$$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E) \quad \lambda_c = 0.656$$

$$N_y = F \times A = \boxed{17365.92 \text{ KN}}$$

$$N_{Ex} = \pi^2 \times E \times I / (k c^2 \times L_{bx}^2) = \boxed{292165.06 \text{ KN}}$$

$$N_{Ey} = \pi^2 \times E \times I / (k c^2 \times L_{by}^2) = \boxed{40326.65 \text{ KN}}$$

$$\text{※、} N_c = \boxed{16718.65 \text{ KN}}$$

$$N / N_y \leq 0.15 : M_{pb} = M_b \quad N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c) \quad N / N_y = 0.000$$

$$M_{pb} = 7052.21 = \boxed{7052.21 \text{ KNm}}$$

使用部材 BH- 1300 x 350 x 16.0 x 32.0 $Z_x = 17728.3 \text{ cm}^3$ $I_x = 1152337 \text{ cm}^4$ $A = 421.76 \text{ cm}^2$

H形強軸 $Z_p = 20470.6 \text{ cm}^3$ $I_y = 22909 \text{ cm}^4$ $i_y = 10.11 \text{ cm}$ $k_c = 1.00$

○ 2G6 中央 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$
Y2-4

強度割増 = 1.1 倍 $L_{bx} = 1000.00 \text{ cm}$
 $L_{by} = 500.00 \text{ cm}$
 $(M_2 / M_1) = 0.000$

部材種別 = 鉛直軸力 = 0.00 KN

$$M_b = \min \{ M_p, M_{LB}, M_{FTB} \} \quad \text{※、角型鋼の場合は、} M_p \text{ のみ考慮。}$$

$$M_p = F \times Z_p = \boxed{5291.65 \text{ KNm}}$$

$$M_{FTB} = p \lambda b \geq \lambda b: M_{FTB} = M_p \quad e \lambda b \geq \lambda b > p \lambda b: (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b]) /$$

$$(1.29 - P \lambda b)) \times M_p \quad \lambda b > e \lambda b: M_p / \lambda b^2 = \boxed{5291.65 \text{ KNm}}$$

$$M_e = C \times Z \times \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)} = \boxed{47270.68 \text{ KNm}}$$

$$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30 \quad \rightarrow \rightarrow C = 1.75$$

$$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 23.52 \text{ KN/cm}^2$$

$$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 150.54 \text{ KN/cm}^2 \quad e \lambda b = 1.29$$

$$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.600 \quad \lambda b = \sqrt{M_p / M_e} = 0.33$$

$$M_{LB} = (1 - N / N_{LB}) \times Z \times \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$$

$$= Z \times \min \{ 300.93, 248.92 \} = \boxed{4412.83 \text{ KNm}}$$

$$N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = \boxed{5671.55 \text{ KN}}$$

$$\text{※、上記結果により } M_b = \boxed{4412.83 \text{ KNm}}$$