

$$N_c = \min(N_y, (1.07 - 0.44\sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$$

$$\lambda_c = 0.758$$

$$N_y = F \times A = \boxed{10902.50 \text{ KN}}$$

$$N_{Ex} = \pi^2 \times E \times I / (k^2 \times L \times b^2) = \boxed{238835.29 \text{ KN}}$$

$$N_{Ey} = \pi^2 \times E \times I / (k^2 \times L \times b^2) = \boxed{18992.51 \text{ KN}}$$

$$\text{※、} N_c = \boxed{10640.75 \text{ KN}}$$

$$N/N_y \leq 0.15 : M_{pb} = M_b \quad N/N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N/N_c) \quad N/N_y = 0.000$$

$$M_{pb} = 4412.83 = \boxed{\boxed{4412.83 \text{ KNm}}}$$

使用部材 BH- 700 x 450 x 16.0 x 36.0  $Z_x = 11157.1 \text{ cm}^3$   $I_x = 390499 \text{ cm}^4$   $A = 424.48 \text{ cm}^2$   
H形強軸  $Z_p = 12424.8 \text{ cm}^3$   $I_y = 54696 \text{ cm}^4$   $k_c = 1.00$   
 $* i_y = 12.99 \text{ cm}$

○ 2G7 端部 (SM50A)

$F = 325 \text{ N/mm}^2$   $F_u = 490 \text{ N/mm}^2$   
強度割増 = 1.1 倍  $L_{bx} = 1000.00 \text{ cm}$   
 $L_{by} = 250.00 \text{ cm}$   
 $(M_2 / M_1) = -0.500$

部材種別 =  鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$  ※、角型鋼の場合は、 $M_p$  のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b: M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b: (1 - 0.4 \times [(\sqrt{M_p/M_e}) - p \lambda b]) / (1.29 - p \lambda b) \times M_p$   $\lambda b > e \lambda b: M_p / \lambda b^2 =$

$M_e = C \times Z_x \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$  →→  $C = 1.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 126.36 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / * i_y)^2 = 994.96 \text{ KN/cm}^2$   $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.450$   $\lambda b = \sqrt{M_p/M_e} = 0.17$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \min \{ 394.56, 387.83 \} =$   ←← FA、FBは省略  
 $N_{LB} = N_y / (0.60 + 1.60 \times F_yf / E \times (b / t_f)^2 + 0.15 \times F_yw / E \times (d / t_w)^2) = 10602.80 \text{ KN}$

※、上記結果により  $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$   
 $\lambda_c = 0.433$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k c^2 \times L_{by}^2) =$

※、 $N_c =$

$N/N_y \leq 0.15 : M_{pb} = M_b$   $N/N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$   $N / N_y = 0.000$

$M_{pb} = 4441.85 =$

使用部材 BH- 700 x 400 x 16.0 x 36.0  $Z_x = 10022.3 \text{ cm}^3$   $I_x = 350779 \text{ cm}^4$   $A = 388.48 \text{ cm}^2$   
H形強軸  $Z_p = 11229.6 \text{ cm}^3$  \*  $i_y = 11.55 \text{ cm}$   $k_c = 1.00$   
○ 2G7 中央  $F = 235 \text{ N/mm}^2$   $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍  $L_{bx} = 1000.00 \text{ cm}$   
 $L_{by} = 250.00 \text{ cm}$   
 $(M_2 / M_1) = 0.000$

部材種別 =  鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$  ※、角型鋼の場合は、 $M_p$  のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b : M_{FTB} = M_p - e \lambda b \geq \lambda b > p \lambda b : (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b] / (1.29 - p \lambda b)) \times M_p$   $\lambda b > e \lambda b : M_p / \lambda b^2 =$

$M_e = C \times Z_x \times \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$   $\rightarrow \rightarrow C = 1.75$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 112.32 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 786.17 \text{ KN/cm}^2$   $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.600$   $\lambda b = \sqrt{M_p / M_e} = 0.14$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \times \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \times \min \{ 300.21, 287.44 \} =$   ←← FA、FBは省略  
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 8790.94 \text{ KN}$

※、上記結果により  $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$   
 $\lambda_c = 0.372$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b$   $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$   $N / N_y = 0.000$

$M_{pb} = 2902.84 =$

使用部材 BH- 700 x 450 x 16.0 x 36.0  $Z_x = 11157.1 \text{ cm}^3$   $I_x = 390499 \text{ cm}^4$   $A = 424.48 \text{ cm}^2$   
 H形強軸  $Z_p = 12424.8 \text{ cm}^3$   $I_y = 54696 \text{ cm}^4$   $k_c = 1.00$   
 $* i_y = 12.99 \text{ cm}$

○ 2G8 端部 (SM50A)

$F = 325 \text{ N/mm}^2$   $F_u = 490 \text{ N/mm}^2$   
 強度割増 = 1.1 倍  $L_{bx} = 1000.00 \text{ cm}$   
 $L_{by} = 250.00 \text{ cm}$   
 $(M_2 / M_1) = -0.500$

部材種別 =  鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$  ※、角型鋼の場合は、 $M_p$  のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b: M_{FTB} = M_p \quad e \lambda b \geq \lambda b > p \lambda b: (1 - 0.4 \times [ ((\sqrt{M_p/M_e}) - p \lambda b) / (1.29 - p \lambda b) ]) \times M_p$   
 $\lambda b > e \lambda b: M_p / \lambda b^2 =$

$M_e = C \times Z_x \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$   $\rightarrow C = 1.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 126.36 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / * i_y)^2 = 994.96 \text{ KN/cm}^2$   $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.450$   $\lambda b = \sqrt{M_p/M_e} = 0.17$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \min \{ 394.56, 387.83 \} =$   ←← FA、FBは省略  
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 10602.80 \text{ KN}$

※、上記結果により  $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$   
 $\lambda_c = 0.433$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k c^2 \times L_{by}^2) =$

※、 $N_c =$

$N/N_y \leq 0.15 : M_{pb} = M_b$   $N/N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N/N_y) = 0.000$

$M_{pb} = 4441.85 =$

使用部材 BH- 700 x 450 x 16.0 x 36.0  $Z_x = 11157.1 \text{ cm}^3$   $I_x = 390499 \text{ cm}^4$   $A = 424.48 \text{ cm}^2$   
H形強軸  $Z_p = 12424.8 \text{ cm}^3$  \*  $i_y = 12.99 \text{ cm}$   $k_c = 1.00$   
○ 2G8 中央  $F = 235 \text{ N/mm}^2$   $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍  $L_{bx} = 1000.00 \text{ cm}$   
 $L_{by} = 250.00 \text{ cm}$   
 $(M_2 / M_1) = 0.000$

部材種別 =  鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$  ※、角型鋼の場合は、 $M_p$  のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b : M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b : (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b] / (1.29 - p \lambda b)) \times M_p$   $\lambda b > e \lambda b : M_p / \lambda b^2 =$

$M_e = C \times Z \times \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$   $\rightarrow C = 1.75$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 126.36 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 994.96 \text{ KN/cm}^2$   $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.600$   $\lambda b = \sqrt{M_p / M_e} = 0.13$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \min \{ 294.44, 287.44 \} =$   ←← FA、FBは省略  
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 9136.01 \text{ KN}$

※、上記結果により  $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$   
 $\lambda_c = 0.368$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b$   $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$   $N / N_y = 0.000$

$M_{pb} = 3211.8 =$

使用部材 H- 692 x 300 x 13.0 x 20.0  $Z_x = 4820.0 \text{ cm}^3$   $I_x = 168000 \text{ cm}^4$   $A = 207.50 \text{ cm}^2$   
H形強軸  $I_y = 9020 \text{ cm}^4$   
 $Z_p = 5500.0 \text{ cm}^3$  \*  $i_y = 7.81 \text{ cm}$   $k_c = 1.00$   
○ 2G9 端部、中央  $F = 235 \text{ N/mm}^2$   $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍  $L_{bx} = 1400.00 \text{ cm}$   
 $L_{by} = 1400.00 \text{ cm}$   
 $(M_2 / M_1) = 1.000$

部材種別 =  鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$  ※、角型鋼の場合は、 $M_p$  のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b : M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b : (1 - 0.4 \times [(\sqrt{M_p/M_e}) - p \lambda b]) / (1.29 - p \lambda b) \times M_p$   $\lambda b > e \lambda b : M_p / \lambda b^2 =$

$M_e = C \times Z_x \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30 \rightarrow C = 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 8.45 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 11.47 \text{ KN/cm}^2$   $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.900$   $\lambda b = \sqrt{M_p/M_e} = 0.95$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \min \{ 284.05, 276.38 \} =$   ←← FA、FBは省略  
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 3627.96 \text{ KN}$

※、上記結果により  $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$   
 $\lambda_c = 2.371$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b$   $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$   $N / N_y = 0.000$

$M_{pb} = 1350.59 =$



使用部材 H- 700 x 300 x 13.0 x 24.0  $Z_x = 5640.0 \text{ cm}^3$   $I_x = 197000 \text{ cm}^4$   $A = 231.50 \text{ cm}^2$   
 H形強軸  $Z_p = 6340.0 \text{ cm}^3$  \*  $I_y = 10800 \text{ cm}^4$   $k_c = 1.00$   
 ○ 2G10 中央  $F = 235 \text{ N/mm}^2$   $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍  $L_{bx} = 1400.00 \text{ cm}$   
 $L_{by} = 1400.00 \text{ cm}$   
 $(M_2 / M_1) = 1.000$

部材種別 =  鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$  ※、角型鋼の場合は、 $M_p$  のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b : M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b : (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b]) / (1.29 - p \lambda b) \times M_p$   $\lambda b > e \lambda b : M_p / \lambda b^2 =$

$M_e = C \times Z_x \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30 \rightarrow C = 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 10.03 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 11.88 \text{ KN/cm}^2$   $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.900$   $\lambda b = \sqrt{M_p / M_e} = 0.90$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \min \{ 294.44, 276.38 \} =$   ←← FA、FBは省略  
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 4379.44 \text{ KN}$

※、上記結果により  $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$   
 $\lambda_c = 2.289$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b$   $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$   $N / N_y = 0.000$

$M_{pb} = 1636.49 =$

使用部材 H- 800 x 300 x 14.0 x 26.0  $Z_x = 7160.0 \text{ cm}^3$   $I_x = 286000 \text{ cm}^4$   $A = 263.50 \text{ cm}^2$   
 $I_y = 11700 \text{ cm}^4$   
 H形強軸  $Z_p = 8100.0 \text{ cm}^3$  \*  $i_y = 7.87 \text{ cm}$   $kc = 1.00$   
 ○ 2G11 端部  $F = 235 \text{ N/mm}^2$   $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍  $L_{bx} = 1400.00 \text{ cm}$   
 $L_{by} = 1400.00 \text{ cm}$   
 $(M_2 / M_1) = 1.000$

部材種別 = FA 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$  ※、角型鋼の場合は、 $M_p$ のみ考慮。

$M_p = F \times Z_p =$  2093.85 KNm

$M_{FTB} = p \lambda b \geq \lambda b : M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b : (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b] / (1.29 - p \lambda b)) \times M_p$   $\lambda b > e \lambda b : M_p / \lambda b^2 =$  2051.52 KNm

$M_e = C \times Z_x \times \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$  2475.38 KNm

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30 \rightarrow C = 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 9.51 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times F / (k \cdot I_{by} / * i_y)^2 = 11.64 \text{ KN/cm}^2$   $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.900$   $\lambda b = \sqrt{M_p / M_e} = 0.92$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \times \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \times \min \{ 298.43, 273.06 \} =$  ----- ←← FA、FBは省略  
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 4912.78 \text{ KN}$

※、上記結果により  $M_b =$  2051.52 KNm

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$   
 $\lambda_c = 2.346$

$N_y = F \times A =$  6811.48 KN

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) =$  30243.29 KN

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) =$  1237.23 KN

※、 $N_c =$  1026.90 KN

$N / N_y \leq 0.15 : M_{pb} = M_b$   $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$   $N / N_y = 0.000$

$M_{pb} = 2051.52 =$  2051.52 KNm

使用部材 H- 792 x 300 x 14.0 x 22.0  $Z_x = 6270.0 \text{ cm}^3$   $I_x = 248000 \text{ cm}^4$   $A = 239.50 \text{ cm}^2$   
H形強軸  $Z_p = 7140.0 \text{ cm}^3$  \*  $I_y = 9920 \text{ cm}^4$   $k_c = 1.00$   
○ 2G11 中央  $F = 235 \text{ N/mm}^2$   $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍  $L_{bx} = 1400.00 \text{ cm}$   
 $L_{by} = 1400.00 \text{ cm}$   
 $(M_2 / M_1) = 1.000$

部材種別 =  鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$  ※、角型鋼の場合は、 $M_p$  のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b : M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b : (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b]) / (1.29 - p \lambda b) \times M_p$   $\lambda b > e \lambda b : M_p / \lambda b^2 =$

$M_e = C \times Z_x \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30 \rightarrow C = 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 8.13 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 11.26 \text{ KN/cm}^2$   $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.900$   $\lambda b = \sqrt{M_p / M_e} = 0.96$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \min \{ 289.72, 273.06 \} =$   ←← FA、FBは省略  
 $N_{LB} = N_y / (0.60 + 1.60 \times F_y f / E \times (b / t_f)^2 + 0.15 \times F_y w / E \times (d / t_w)^2) = 4211.22 \text{ KN}$

※、上記結果により  $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$   
 $\lambda_c = 2.429$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b$   $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$   $N / N_y = 0.000$

$M_{pb} = 1732.09 =$

使用部材 BH- 692 x 400 x 12.0 x 22.0  $Z_x = 6497.0 \text{ cm}^3$   $I_x = 224797 \text{ cm}^4$   $A = 253.76 \text{ cm}^2$   
 H形強軸  $Z_p = 7198.5 \text{ cm}^3$  \*  $i_y = 7.74 \text{ cm}$   $k_c = 1.00$   
 ○ 2G12 端部 (SM50A)  $F = 325 \text{ N/mm}^2$   $F_u = 490 \text{ N/mm}^2$   
 強度割増 = 1.1 倍  $L_{bx} = 1400.00 \text{ cm}$   
 $L_{by} = 1400.00 \text{ cm}$   
 $(M_2 / M_1) = 1.000$

部材種別 =  鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$  ※、角型鋼の場合は、 $M_p$ のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b : M_{FTB} = M_p \quad e \lambda b \geq \lambda b > p \lambda b : (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b]) /$   
 $(1.29 - p \lambda b)] \times M_p \quad \lambda b > e \lambda b : M_p / \lambda b^2 =$

$M_e = C \times Z_x \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30 \quad \rightarrow \rightarrow C = 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 12.40 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 11.26 \text{ KN/cm}^2 \quad e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.900 \quad \lambda b = \sqrt{M_p / M_e} = 1.01$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \min \{ 356.15, 363.52 \} =$   ←← FA、FBは省略  
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 4141.38 \text{ KN}$

※、上記結果により  $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$   
 $\lambda_c = 1.912$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b \quad N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c) \quad N / N_y = 0.000$

$M_{pb} = 2272.62 =$

使用部材 H- 692 x 300 x 13.0 x 20.0  $Z_x = 4870.0 \text{ cm}^3$   $I_x = 168000 \text{ cm}^4$   $A = 207.50 \text{ cm}^2$   
 $I_y = 9020 \text{ cm}^4$   
 H形強軸  $Z_p = 5500.0 \text{ cm}^3$  \*  $i_y = 7.81 \text{ cm}$   $kc = 1.00$   
 ○ 2G12 中央  $F = 325 \text{ N/mm}^2$   $F_u = 490 \text{ N/mm}^2$   
 (SM50A)  
 強度割増 = 1.1 倍  $L_{bx} = 1400.00 \text{ cm}$   
 $L_{by} = 1400.00 \text{ cm}$   
 $(M_2 / M_1) = 1.000$

部材種別 =  鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$  ※、角型鋼の場合は、 $M_p$  のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b : M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b : (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b]) /$   
 $(1.29 - p \lambda b)] \times M_p \quad \lambda b > e \lambda b : M_p / \lambda b^2 =$

$M_e = C \times Z_x \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30 \quad \rightarrow \rightarrow C = 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 8.45 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 11.47 \text{ KN/cm}^2 \quad e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.900 \quad \lambda b = \sqrt{M_p / M_e} = 1.11$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \min \{ 377.66, 369.86 \} =$   ←← FA、FBは省略  
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 4087.29 \text{ KN}$

※、上記結果により  $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$   
 $\lambda_c = 2.789$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b \quad N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c) \quad N / N_y = 0.000$

$M_{pb} = 1542.65 =$

使用部材 H- 350 x 175 x 7.0 x 11.0  $Z_x = 771.0 \text{ cm}^3$   $I_x = 13500 \text{ cm}^4$   $A = 62.91 \text{ cm}^2$   
 H形強軸  $Z_p = 864.0 \text{ cm}^3$   $I_y = 984 \text{ cm}^4$   $* i_y = 4.60 \text{ cm}$   $kc = 1.00$   
 ○ 2G14 端部、中央  $F = 235 \text{ N/mm}^2$   $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍  $L_{bx} = 500.00 \text{ cm}$   
 $L_{by} = 500.00 \text{ cm}$   
 $(M_2 / M_1) = 1.000$

部材種別 = FA 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$  ※、角型鋼の場合は、 $M_p$ のみ考慮。

$M_p = F \times Z_p =$  223.34 KNm

$M_{FTB} = p \lambda b \geq \lambda b: M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b: (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b] / (1.29 - p \lambda b)) \times M_p$   $\lambda b > e \lambda b: M_p / \lambda b^2 =$  223.34 KNm

$M_e = C \times Z_x \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$  613.80 KNm

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30 \rightarrow C = 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 15.02 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / * i_y)^2 = 31.19 \text{ KN/cm}^2$   $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.900$   $\lambda b = \sqrt{M_p / M_e} = 0.60$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \min \{ 280.27, 279.72 \} =$  ----- ←← FA、FBは省略  
 $N_{LB} = N_y / (0.60 + 1.60 * F_{yf} / E * (b / t_f)^2 + 0.15 * F_{yw} / E * (d / t_w)^2) = 1104.16 \text{ KN}$

※、上記結果により  $M_b =$  223.34 KNm

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$   
 $\lambda_c = 1.412$

$N_y = F \times A =$  1626.22 KN

$N_{Ex} = \pi^2 \times E \times I / (k c^2 \times L_{bx}^2) =$  11192.13 KN

$N_{Ey} = \pi^2 \times E \times I / (k c^2 \times L_{by}^2) =$  815.78 KN

※、 $N_c =$  677.10 KN

$N / N_y \leq 0.15 : M_{pb} = M_b$   $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$   $N / N_y = 0.000$

$M_{pb} = 223.34 =$  223.34 KNm

使用部材 BH- 1300 x 450 x 16.0 x 28.0  $Z_x = 19633.5 \text{ cm}^3$   $I_x = 1276179 \text{ cm}^4$   $A = 451.04 \text{ cm}^2$   
H形強軸  $Z_p = 22356.7 \text{ cm}^3$   $I_y = 42567 \text{ cm}^4$   $l_y = 12.99 \text{ cm}$   $kc = 1.00$

○ 2G15 端部 (SM50A)

$F = 325 \text{ N/mm}^2$   $F_u = 490 \text{ N/mm}^2$

強度割増 = 1.1 倍  $L_{bx} = 1000.00 \text{ cm}$   
 $L_{by} = 250.00 \text{ cm}$   
 $(M_2 / M_1) = -0.500$

部材種別 =  鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$  ※、角型鋼の場合は、 $M_p$  のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b : M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b : (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b]) / (1.29 - p \lambda b) \times M_p$   $\lambda b > e \lambda b : M_p / \lambda b^2 =$

$M_e = C \times Z_x \times \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$   $\rightarrow \rightarrow C = 1.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 52.92 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 995.16 \text{ KN/cm}^2$   $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.450$   $\lambda b = \sqrt{M_p / M_e} = 0.18$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \times \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \times \min \{ 370.42, 324.36 \} =$

$N_{LB} = N_y / (0.60 + 1.60 \times F_y f / E \times (b / t_f)^2 + 0.15 \times F_y w / E \times (d / t_w)^2) =$

※、上記結果により  $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$

$\lambda_c = 0.338$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b$   $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$   $N / N_y = 0.000$

$M_{pb} = 6368.32 =$

使用部材 BH- 1300 x 300 x 16.0 x 28.0  $Z_x = 14405.3 \text{ cm}^3$   $I_x = 936348 \text{ cm}^4$   $A = 367.04 \text{ cm}^2$   
H形強軸  $Z_p = 17014.3 \text{ cm}^3$   $I_y = 12642 \text{ cm}^4$   $k_c = 1.00$   
○ 2G15 中央  $F = 235 \text{ N/mm}^2$   $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍  $L_{bx} = 1000.00 \text{ cm}$   
 $L_{by} = 250.00 \text{ cm}$   
 $(M_2 / M_1) = 0.000$

部材種別 =  鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$  ※、角型鋼の場合は、 $M_p$  のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b : M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b : (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b]) / (1.29 - p \lambda b) \times M_p$   
 $\lambda b > e \lambda b : M_p / \lambda b^2 =$

$M_e = C \times Z_x \times \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$  →→  $C = 1.75$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 35.28 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 442.61 \text{ KN/cm}^2$   $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.600$   $\lambda b = \sqrt{M_p / M_e} = 0.20$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \times \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \times \min \{ 301.86, 248.41 \} =$    
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 4958.03 \text{ KN}$

※、上記結果により  $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$   
 $\lambda_c = 0.476$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b$   $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$   $N / N_y = 0.000$

$M_{pb} = 3578.41 =$

使用部材 BH- 900 x 450 x 16.0 x 32.0  $Z_x = 13791.4 \text{ cm}^3$   $I_x = 620615 \text{ cm}^4$   $A = 421.76 \text{ cm}^2$   
H形強軸  $Z_p = 15401.8 \text{ cm}^3$  \*  $i_y = 12.99 \text{ cm}$   $k_c = 1.00$   
○ 2G16 端部  $F = 235 \text{ N/mm}^2$   $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍  $L_{bx} = 1200.00 \text{ cm}$   
 $L_{by} = 1200.00 \text{ cm}$   
 $(M_2 / M_1) = 1.000$

部材種別 =  鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$  ※、角型鋼の場合は、 $M_p$  のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b : M_{FTB} = M_p - e \lambda b \geq \lambda b > p \lambda b : (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b]) / (1.29 - p \lambda b) \times M_p$   $\lambda b > e \lambda b : M_p / \lambda b^2 =$

$M_e = C \times Z_x \times \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30 \rightarrow C = 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 18.20 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 43.19 \text{ KN/cm}^2$   $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.900$   $\lambda b = \sqrt{M_p / M_e} = 0.52$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \times \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \times \min \{ 287.94, 274.26 \} =$   ←← FA、FBは省略  
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 7340.84 \text{ KN}$

※、上記結果により  $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$   
 $\lambda_c = 1.248$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b$   $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$   $N / N_y = 0.000$

$M_{pb} = 3981.36 =$

使用部材 H- 900 x 300 x 16.0 x 28.0  $Z_x = 8990.0 \text{ cm}^3$   $I_x = 404000 \text{ cm}^4$   $A = 305.80 \text{ cm}^2$   
H形強軸  $Z_p = 10300.0 \text{ cm}^3$   $I_y = 12600 \text{ cm}^4$   $k_c = 1.00$   
○ 2G16 中央  $F = 235 \text{ N/mm}^2$   $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍  $L_{bx} = 1200.00 \text{ cm}$   
 $L_{by} = 1200.00 \text{ cm}$   
 $(M_2 / M_1) = 1.000$

部材種別 =  鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$  ※、角型鋼の場合は、 $M_p$  のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b : M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b : (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b] / (1.29 - p \lambda b)) \times M_p$   $\lambda b > e \lambda b : M_p / \lambda b^2 =$

$M_e = C \times Z_x \times \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$   $\rightarrow C = 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 10.62 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 15.37 \text{ KN/cm}^2$   $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.900$   $\lambda b = \sqrt{M_p / M_e} = 0.83$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \times \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \times \min \{ 301.86, 273.75 \} =$   ←← FA, FBは省略  
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 5913.99 \text{ KN}$

※、上記結果により  $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$   
 $\lambda_c = 2.088$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b$   $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$   $N / N_y = 0.000$

$M_{pb} = 2662.55 =$

使用部材 H- 800 x 300 x 14.0 x 26.0  $Z_x = 7160.0 \text{ cm}^3$   $I_x = 286000 \text{ cm}^4$   $A = 263.50 \text{ cm}^2$   
H形強軸  $Z_p = 8100.0 \text{ cm}^3$   $I_y = 11700 \text{ cm}^4$   $k_c = 1.00$   
○ 2G17 端部  $F = 235 \text{ N/mm}^2$   $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍  $L_{bx} = 1200.00 \text{ cm}$   
 $L_{by} = 1200.00 \text{ cm}$   
 $(M_2 / M_1) = 1.000$

部材種別 =  鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$  ※、角型鋼の場合は、 $M_p$  のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b : M_{FTB} = M_p \quad e \lambda b > p \lambda b : (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b] / (1.29 - p \lambda b)) \times M_p$   
 $\lambda b > e \lambda b : M_p / \lambda b^2 =$

$M_e = C \times Z \times \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30 \rightarrow C = 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 11.09 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 15.85 \text{ KN/cm}^2 \quad e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.900 \quad \lambda b = \sqrt{M_p / M_e} = 0.81$

$M_{LB} = (1 - N / N_{LB}) \times Z \times \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z \times \min \{ 298.43, 273.06 \} =$   ←← FA、FBは省略  
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 4912.78 \text{ KN}$

※、上記結果により  $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$   
 $\lambda_c = 2.011$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b \quad N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_y) \quad N / N_y = 0.000$

$M_{pb} = 2093.85 =$

使用部材 H- 792 x 300 x 14.0 x 22.0  $Z_x = 6270.0 \text{ cm}^3$   $I_x = 248000 \text{ cm}^4$   $A = 239.50 \text{ cm}^2$   
H形強軸  $Z_p = 7140.0 \text{ cm}^3$   $I_y = 9920 \text{ cm}^4$   $k_c = 1.00$   
○ 2G17 中央  $F = 235 \text{ N/mm}^2$   $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍  $L_{bx} = 1200.00 \text{ cm}$   
 $L_{by} = 1200.00 \text{ cm}$   
 $(M_2 / M_1) = 1.000$

部材種別 = FA 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$  ※、角型鋼の場合は、 $M_p$  のみ考慮。

$M_p = F \times Z_p =$  1845.69 KNm

$M_{FTB} = p \lambda b \geq \lambda b: M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b: (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b] / (1.29 - p \lambda b)) \times M_p$   
 $\lambda b > e \lambda b: M_p / \lambda b^2 =$  1845.69 KNm

$M_e = C \times Z_x \times \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$  2599.12 KNm

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30 \rightarrow C = 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 9.48 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 15.33 \text{ KN/cm}^2$   $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.900$   $\lambda b = \sqrt{M_p / M_e} = 0.84$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \times \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \times \min \{ 289.72, 273.06 \} =$  ----- ←← FA、FBは省略

$N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 4211.22 \text{ KN}$

※、上記結果により  $M_b =$  1845.69 KNm

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$   
 $\lambda_c = 2.082$

$N_y = F \times A =$  6191.08 KN

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) =$  35695.07 KN

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) =$  1427.80 KN

※、 $N_c =$  1185.08 KN

$N / N_y \leq 0.15 : M_{pb} = M_b$   $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$   $N / N_y = 0.000$

$M_{pb} = 1845.69 =$  1845.69 KNm

使用部材 H- 800 x 300 x 14.0 x 26.0  $Z_x = 7160.0 \text{ cm}^3$   $I_x = 286000 \text{ cm}^4$   $A = 263.50 \text{ cm}^2$   
H形強軸  $Z_p = 8100.0 \text{ cm}^3$   $I_y = 11700 \text{ cm}^4$   $k_c = 1.00$   
○ 2G17 端部  $F = 235 \text{ N/mm}^2$   $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍  $L_{bx} = 1400.00 \text{ cm}$   
 $L_{by} = 1400.00 \text{ cm}$   
 $(M_2 / M_1) = 1.000$

部材種別 =  鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$  ※、角型鋼の場合は、 $M_p$  のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b: M_{FTB} = M_p \quad e \lambda b \geq \lambda b > p \lambda b: (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b]) / (1.29 - P \lambda b) \times M_p$   
 $\lambda b > e \lambda b: M_p / \lambda b^2 =$

$M_e = C \times Z_x \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30 \rightarrow C = 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 9.51 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 11.64 \text{ KN/cm}^2 \quad e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.900 \quad \lambda b = \sqrt{M_p / M_e} = 0.92$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \min \{ 298.43, 273.06 \} =$   ←← FA、FBは省略  
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 4912.78 \text{ KN}$

※、上記結果により  $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$   
 $\lambda_c = 2.346$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b \quad N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c) \quad N / N_y = 0.000$

$M_{pb} = 2051.52 =$

使用部材 H- 792 x 300 x 14.0 x 22.0  $Z_x = 6270.0 \text{ cm}^3$   $I_x = 248000 \text{ cm}^4$   $A = 239.50 \text{ cm}^2$   
H形強軸  $Z_p = 7140.0 \text{ cm}^3$   $I_y = 9920 \text{ cm}^4$   $k_c = 1.00$   
○ 2G17 中央  $F = 235 \text{ N/mm}^2$   $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍  $L_{bx} = 1400.00 \text{ cm}$   
 $L_{by} = 1400.00 \text{ cm}$   
 $(M_2 / M_1) = 1.000$

部材種別 =  鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$  ※、角型鋼の場合は、 $M_p$  のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b : M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b : (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b] / (1.29 - p \lambda b)) \times M_p$   $\lambda b > e \lambda b : M_p / \lambda b^2 =$

$M_e = C \times Z_x \times \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30 \rightarrow C = 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 8.13 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 11.26 \text{ KN/cm}^2$   $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.900$   $\lambda b = \sqrt{M_p / M_e} = 0.96$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \times \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \times \min \{ 289.72, 273.06 \} =$   ←← FA、FBは省略  
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 4211.22 \text{ KN}$

※、上記結果により  $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$   
 $\lambda_c = 2.429$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b$   $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$   $N / N_y = 0.000$

$M_{pb} = 1732.09 =$

使用部材 BH- 800 x 450 x 16.0 x 28.0  $Z_x = 10763.6 \text{ cm}^3$   $I_x = 430545 \text{ cm}^4$   $A = 371.04 \text{ cm}^2$   
H形強軸  $Z_p = 12024.7 \text{ cm}^3$   $I_y = 42550 \text{ cm}^4$   $k_c = 1.00$   
○ 2G18 端部  $F = 235 \text{ N/mm}^2$   $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍  $L_{bx} = 1400.00 \text{ cm}$   
 $L_{by} = 1400.00 \text{ cm}$   
 $(M_2 / M_1) = 1.000$

部材種別 =  鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$  ※、角型鋼の場合は、 $M_p$  のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b: M_{FTB} = M_p \quad e \lambda b \geq \lambda b > p \lambda b: (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b]) / (1.29 - p \lambda b)$   
 $\lambda b > e \lambda b: M_p / \lambda b^2 =$

$M_e = C \times Z_x \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30 \rightarrow C = 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 15.36 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 31.73 \text{ KN/cm}^2 \quad e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.900 \quad \lambda b = \sqrt{M_p / M_e} = 0.60$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \min \{ 279.59, 280.09 \} =$   ←← FA、FBは省略  
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 6471.45 \text{ KN}$

※、上記結果により  $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$   
 $\lambda_c = 1.460$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b \quad N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c) \quad N / N_y = 0.000$

$M_{pb} = 3108.38 =$