

使用部材 H- 692 x 300 x 13.0 x 20.0 $Z_x = 4870.0 \text{ cm}^3$ $I_x = 168000 \text{ cm}^4$ $A = 207.50 \text{ cm}^2$
H形強軸 $I_y = 9020 \text{ cm}^4$
 $Z_p = 5500.0 \text{ cm}^3$ * $i_y = 7.81 \text{ cm}$ $kc = 1.00$
○ R1G7 端部 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{bx} = 1450.00 \text{ cm}$
 $L_{by} = 1450.00 \text{ cm}$
 $(M_2 / M_1) = 1.000$

部材種別 = 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b: M_{FTB} = M_p \quad e \lambda b \geq \lambda b > p \lambda b: (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b]) / (1.29 - p \lambda b) \times M_p$
 $\lambda b > e \lambda b: M_p / \lambda b^2 =$

$M_e = C \times Z_x \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30 \rightarrow C = 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 8.16 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 10.69 \text{ KN/cm}^2 \quad e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.900 \quad \lambda b = \sqrt{M_p / M_e} = 0.97$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \min \{ 284.05, 276.38 \} =$ ← FA、FBは省略
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 3627.96 \text{ KN}$

※、上記結果により $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 2.456$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b \quad N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c) \quad N / N_y = 0.000$

$M_{pb} = 1317.53 =$

使用部材 H- 692 x 300 x 13.0 x 20.0 $Z_x = 4870.0 \text{ cm}^3$ $I_x = 168000 \text{ cm}^4$ $A = 207.50 \text{ cm}^2$
H形強軸 $Z_p = 5500.0 \text{ cm}^3$ $I_y = 9020 \text{ cm}^4$ $* i_y = 7.81 \text{ cm}$ $kc = 1.00$
○ R1G7 中央 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{bx} = 1450.00 \text{ cm}$
 $L_{by} = 1450.00 \text{ cm}$
 $(M_2 / M_1) = 1.000$

部材種別 = 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b : M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b : (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b]) / (1.29 - p \lambda b) \times M_p$ $\lambda b > e \lambda b : M_p / \lambda b^2 =$

$M_e = C \times Z_x \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30 \rightarrow C = 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 8.16 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times F / (k \cdot I_{by} / * i_y)^2 = 10.69 \text{ KN/cm}^2$ $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.900$ $\lambda b = \sqrt{M_p / M_e} = 0.97$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \min \{ 284.05, 276.38 \} =$ ←← FA、FBは省略
 $N_{LB} = N_y / (0.60 + 1.60 \times F_y f / E \times (b / t_f)^2 + 0.15 \times F_y w / E \times (d / t_w)^2) = 3627.96 \text{ KN}$

※、上記結果により $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 2.456$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k \cdot c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k \cdot c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b$ $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.000$

$M_{pb} = 1317.53 =$

使用部材 H- 692 x 300 x 13.0 x 20.0 $Z_x = 4870.0 \text{ cm}^3$ $I_x = 168000 \text{ cm}^4$ $A = 207.50 \text{ cm}^2$
H形強軸 $I_y = 9020 \text{ cm}^4$
 $Z_p = 5500.0 \text{ cm}^3$ * $i_y = 7.81 \text{ cm}$ $k_c = 1.00$
○ R1G7 端部 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{bx} = 1200.00 \text{ cm}$
 $L_{by} = 1200.00 \text{ cm}$
 $(M_2 / M_1) = 1.000$

部材種別 = 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b : M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b : (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b]) / (1.29 - p \lambda b) \times M_p$ $\lambda b > e \lambda b : M_p / \lambda b^2 =$

$M_e = C \times Z_x \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$ →→→ $C = 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 9.86 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 15.61 \text{ KN/cm}^2$ $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.900$ $\lambda b = \sqrt{M_p / M_e} = 0.83$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \min \{ 284.05, 276.38 \} =$ ←← FA、FBは省略
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 3627.96 \text{ KN}$

※、上記結果により $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 2.033$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b$ $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.000$

$M_{pb} = 1421.75 =$

使用部材 H- 692 x 300 x 13.0 x 20.0 $Z_x = 4870.0 \text{ cm}^3$ $I_x = 168000 \text{ cm}^4$ $A = 207.50 \text{ cm}^2$
H形強軸 $Z_p = 5500.0 \text{ cm}^3$ $I_y = 9020 \text{ cm}^4$ $* i_y = 7.81 \text{ cm}$ $kc = 1.00$
○ R1G7 中央 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{bx} = 1200.00 \text{ cm}$
 $L_{by} = 1200.00 \text{ cm}$
 $(M_2 / M_1) = 1.000$

部材種別 = FA 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$ 1421.75 KNm

$M_{FTB} = p \lambda b \geq \lambda b : M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b : (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b]) / (1.29 - p \lambda b) \times M_p$ $\lambda b > e \lambda b : M_p / \lambda b^2 =$ 1421.75 KNm

$M_e = C \times Z_x \times \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$ 2068.00 KNm

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30 \rightarrow C = 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 9.86 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / * i_y)^2 = 15.61 \text{ KN/cm}^2$ $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.900$ $\lambda b = \sqrt{M_p / M_e} = 0.83$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \times \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \times \min \{ 284.05, 276.38 \} =$ ---- ←← FA、FBは省略
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 3627.96 \text{ KN}$

※、上記結果により $M_b =$ 1421.75 KNm

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 2.033$

$N_y = F \times A =$ 5363.88 KN

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) =$ 24180.53 KN

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) =$ 1298.26 KN

※、 $N_c =$ 1077.56 KN

$N / N_y \leq 0.15 : M_{pb} = M_b$ $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.000$

$M_{pb} = 1421.75 =$ 1421.75 KNm

使用部材 H- 700 x 300 x 13.0 x 24.0 $Z_x = 5640.0 \text{ cm}^3$ $I_x = 197000 \text{ cm}^4$ $A = 231.50 \text{ cm}^2$
H形強軸 $Z_p = 6340.0 \text{ cm}^3$ $I_y = 10800 \text{ cm}^4$ $k_c = 1.00$
○ R1G8 端部 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{bx} = 1200.00 \text{ cm}$
 $L_{by} = 1200.00 \text{ cm}$
 $(M_2 / M_1) = 1.000$

部材種別 = FA 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$ 1638.89 KNm

$M_{FTB} = p \lambda b \geq \lambda b : M_{FTB} = M_p - e \lambda b \geq \lambda b > p \lambda b : (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b] / (1.29 - p \lambda b)) \times M_p$
 $\lambda b > e \lambda b : M_p / \lambda b^2 =$ 1638.89 KNm

$M_e = C \times Z_x \times \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$ 2589.30 KNm

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$ →→ $C = 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 11.70 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 16.17 \text{ KN/cm}^2$ $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.900$ $\lambda b = \sqrt{M_p / M_e} = 0.80$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \times \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \times \min \{ 294.44, 276.38 \} =$ ---- ←← FA、FBは省略
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 4379.44 \text{ KN}$

※、上記結果により $M_b =$ 1638.89 KNm

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 1.962$

$N_y = F \times A =$ 5984.28 KN

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) =$ 28354.55 KN

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) =$ 1554.46 KN

※、 $N_c =$ 1290.20 KN

$N / N_y \leq 0.15 : M_{pb} = M_b$ $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.000$

$M_{pb} = 1638.89 =$ 1638.89 KNm

使用部材 H- 692 x 300 x 13.0 x 20.0 $Z_x = 4870.0 \text{ cm}^3$ $I_x = 168000 \text{ cm}^4$ $A = 207.50 \text{ cm}^2$
H形強軸 $I_y = 9020 \text{ cm}^4$
 $Z_p = 5500.0 \text{ cm}^3$ * $i_y = 7.81 \text{ cm}$ $k_c = 1.00$
○ R1G8 中央 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{bx} = 1200.00 \text{ cm}$
 $L_{by} = 1200.00 \text{ cm}$
 $(M_2 / M_1) = 1.000$

部材種別 = 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b : M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b : (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b] / (1.29 - p \lambda b)) \times M_p$ $\lambda b > e \lambda b : M_p / \lambda b^2 =$

$M_e = C \times Z_x \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$ →→ $C = 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 9.86 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 15.61 \text{ KN/cm}^2$ $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.900$ $\lambda b = \sqrt{M_p / M_e} = 0.83$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \min \{ 284.05, 276.38 \} =$ ←← FA、FBは省略
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 3627.96 \text{ KN}$

※、上記結果により $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 2.033$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b$ $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.000$

$M_{pb} = 1421.75 =$

使用部材 H- 600 x 200 x 11.0 x 17.0 $Z_x = 2520.0 \text{ cm}^3$ $I_x = 75600 \text{ cm}^4$ $A = 131.70 \text{ cm}^2$
 H形強軸 $I_y = 2270 \text{ cm}^4$
 $Z_p = 2900.0 \text{ cm}^3$ * $i_y = 5.09 \text{ cm}$ $k_c = 1.00$
 ○ R1G9 端部 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{bx} = 1600.00 \text{ cm}$
 $L_{by} = 400.00 \text{ cm}$
 $(M_2 / M_1) = -0.500$

部材種別 = 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b: M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b: (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b] / (1.29 - p \lambda b)) \times M_p$
 $\lambda b > e \lambda b: M_p / \lambda b^2 =$

$M_e = C \times Z_x \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$ →→ $C = 1.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 19.34 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 59.66 \text{ KN/cm}^2$ $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.450$ $\lambda b = \sqrt{M_p / M_e} = 0.60$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \min \{ 297.49, 275.06 \} =$ ←← FA、FBは省略
 $N_{LB} = N_y / (0.60 + 1.60 \times F_y f / E \times (b / t_f)^2 + 0.15 \times F_y w / E \times (d / t_w)^2) = 2527.00 \text{ KN}$

※、上記結果により $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 1.076$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b$ $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.000$

$M_{pb} = 694.67 =$

使用部材 H- 600 x 200 x 11.0 x 17.0 $Z_x = 2520.0 \text{ cm}^3$ $I_x = 75600 \text{ cm}^4$ $A = 131.70 \text{ cm}^2$
H形強軸 $Z_p = 2900.0 \text{ cm}^3$ $I_y = 2270 \text{ cm}^4$ $* i_y = 5.09 \text{ cm}$ $kc = 1.00$
○ RIG9 中央 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{bx} = 1600.00 \text{ cm}$
 $L_{by} = 400.00 \text{ cm}$
 $(M_2 / M_1) = 0.000$

部材種別 = 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b : M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b : (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b] / (1.29 - p \lambda b)) \times M_p$ $\lambda b > e \lambda b : M_p / \lambda b^2 =$

$M_e = C \times Z_x \times \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$ $\rightarrow \rightarrow C = 1.75$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 19.34 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / * i_y)^2 = 59.66 \text{ KN/cm}^2$ $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.600$ $\lambda b = \sqrt{M_p / M_e} = 0.52$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \times \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \times \min \{ 297.49, 275.06 \} =$ ←← FA、FBは省略
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 2527.00 \text{ KN}$

※、上記結果により $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 1.076$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b$ $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.000$

$M_{pb} = 749.65 =$

使用部材 H- 496 x 199 x 9.0 x 14.0 $Z_x = 1650.0 \text{ cm}^3$ $I_x = 40800 \text{ cm}^4$ $A = 99.29 \text{ cm}^2$
H形強軸 $I_y = 1840 \text{ cm}^4$
 $Z_p = 1870.0 \text{ cm}^3$ * $i_y = 5.14 \text{ cm}$ $k_c = 1.00$
○ R1G10 端部 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{bx} = 1200.00 \text{ cm}$
 $L_{by} = 400.00 \text{ cm}$
 $(M_2 / M_1) = -0.666$

部材種別 = 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b : M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b : (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b]) / (1.29 - p \lambda b) \times M_p$ $\lambda b > e \lambda b : M_p / \lambda b^2 =$

$M_e = C \times Z_x \times \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$ $\rightarrow \rightarrow C = 1.18$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 19.17 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 60.84 \text{ KN/cm}^2$ $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.400$ $\lambda b = \sqrt{M_p / M_e} = 0.62$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \times \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \times \min \{ 287.31, 274.51 \} =$ ←← FA、FBは省略
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 1744.14 \text{ KN}$

※、上記結果により $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 1.038$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b$ $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.000$

$M_{pb} = 435.01 =$

使用部材 H- 496 x 199 x 9.0 x 14.0 $Z_x = 1650.0 \text{ cm}^3$ $I_x = 40800 \text{ cm}^4$ $A = 99.29 \text{ cm}^2$
H形強軸 $Z_p = 1870.0 \text{ cm}^3$ $I_y = 1840 \text{ cm}^4$ $l_c = 1.00$
○ R1G10 中央 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{bx} = 12000.00 \text{ cm}$
 $L_{by} = 400.00 \text{ cm}$
 $(M_2 / M_1) = -0.500$

部材種別 = FA 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$ 483.40 KNm

$M_{FTB} = p \lambda b \geq \lambda b: M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b: (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b]) / (1.29 - p \lambda b) \times M_p$
 $\lambda b > e \lambda b: M_p / \lambda b^2 =$ 450.16 KNm

$M_e = C \times Z_x \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$ 1368.29 KNm

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30 \rightarrow C = 1.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 19.17 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 60.84 \text{ KN/cm}^2$ $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.450$ $\lambda b = \sqrt{M_p / M_e} = 0.59$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \min \{ 287.31, 274.51 \} =$ ----- ←← FA、FBは省略
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 1744.14 \text{ KN}$

※、上記結果により $M_b =$ 450.16 KNm

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 6.611$

$N_y = F \times A =$ 2566.65 KN

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) =$ 58.72 KN

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) =$ 2383.51 KN

※、 $N_c =$ -4719.78 KN

$N / N_y \leq 0.15 : M_{pb} = M_b$ $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.000$

$M_{pb} = 450.16 =$ 450.16 KNm

使用部材 H- 606 x 201 x 12.0 x 20.0 $Z_x = 2910.0 \text{ cm}^3$ $I_x = 88300 \text{ cm}^4$ $A = 149.80 \text{ cm}^2$
 H形強軸 $Z_p = 3360.0 \text{ cm}^3$ $I_y = 2720 \text{ cm}^4$ $k_c = 1.00$
 ○ R1G12 端部 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{bx} = 1200.00 \text{ cm}$
 $L_{by} = 1200.00 \text{ cm}$
 $(M_2 / M_1) = 1.000$

部材種別 = 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b : M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b : (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b]) / (1.29 - p \lambda b) \times M_p$ $\lambda b > e \lambda b : M_p / \lambda b^2 =$

$M_e = C \times Z_x \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$ $\rightarrow \rightarrow C = 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 7.55 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 6.84 \text{ KN/cm}^2$ $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.900$ $\lambda b = \sqrt{M_p / M_e} = 1.13$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \min \{ 304.62, 279.41 \} =$ $\leftarrow \leftarrow$ FA、FBは省略
 $N_{LB} = N_y / (0.60 + 1.60 \times F_y f / E \times (b / t_f)^2 + 0.15 \times F_y w / E \times (d / t_w)^2) = 3203.13 \text{ KN}$

※、上記結果により $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 3.145$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b$ $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.000$

$M_{pb} = 664.71 =$

使用部材 H- 596 x 199 x 10.0 x 15.0 $Z_x = 2240.0 \text{ cm}^3$ $I_x = 66600 \text{ cm}^4$ $A = 117.80 \text{ cm}^2$
H形強軸 $Z_p = 2580.0 \text{ cm}^3$ $I_y = 1980 \text{ cm}^4$ $k_c = 1.00$
○ RIG12 中央 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{bx} = 1200.00 \text{ cm}$
 $L_{by} = 1200.00 \text{ cm}$
 $(M_2 / M_1) = 1.000$

部材種別 - FA 鉛直軸力 - 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p = 666.93 \text{ KNm}$

$M_{FTB} = p \lambda b \geq \lambda b : M_{FTB} = M_p - e \lambda b \geq \lambda b > p \lambda b : (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b] / (1.29 - p \lambda b)) \times M_p$
 $\lambda b > e \lambda b : M_p / \lambda b^2 = 444.49 \text{ KNm}$

$M_e = C \times Z_x \times \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)} = 444.29 \text{ KNm}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30 \rightarrow C = 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 5.70 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 6.47 \text{ KN/cm}^2$ $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.900$ $\lambda b = \sqrt{M_p / M_e} = 1.23$

$M_{LB} = (1 - N / N_LB) \times Z_x \times \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \times \min \{ 291.25, 269.85 \} = \text{----}$ ←← FA、FBは省略
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 2014.79 \text{ KN}$

※、上記結果により $M_b = 444.49 \text{ KNm}$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 3.269$

$N_y = F \times A = 3045.13 \text{ KN}$

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) = 9585.85 \text{ KN}$

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) = 284.98 \text{ KN}$

※、 $N_c = 236.54 \text{ KN}$

$N / N_y \leq 0.15 : M_{pb} = M_b$ $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_y) = 0.000$

$M_{pb} = 444.49 = 444.49 \text{ KNm}$

使用部材 H- 606 x 201 x 12.0 x 20.0 $Z_x = 2910.0 \text{ cm}^3$ $I_x = 88300 \text{ cm}^4$ $A = 149.80 \text{ cm}^2$
H形強軸 $I_y = 2720 \text{ cm}^4$
 $Z_p = 3360.0 \text{ cm}^3$ * $i_y = 5.17 \text{ cm}$ $k_c = 1.00$
○ RIG12 端部 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{bx} = 1450.00 \text{ cm}$
 $L_{by} = 1450.00 \text{ cm}$
 $(M_2 / M_1) = 1.000$

部材種別 = 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b: M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b: (1 - 0.4 \times [(\sqrt{M_p/M_e}) - p \lambda b]) / (1.29 - p \lambda b) \times M_p$ $\lambda b > e \lambda b: M_p / \lambda b^2 =$

$M_e = C \times Z_x \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$ $\rightarrow \rightarrow C = 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 6.24 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 4.68 \text{ KN/cm}^2$ $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.900$ $\lambda b = \sqrt{M_p/M_e} = 1.29$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \min \{ 304.62, 279.41 \} =$ ←← FA、FBは省略
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 3203.13 \text{ KN}$

※、上記結果により $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 3.800$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b$ $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.000$

$M_{pb} = 521.73 =$

使用部材 H- 596 x 199 x 10.0 x 15.0 $Z_x = 2240.0 \text{ cm}^3$ $I_x = 66600 \text{ cm}^4$ $A = 117.80 \text{ cm}^2$
H形強軸 $Z_p = 2580.0 \text{ cm}^3$ $I_y = 1980 \text{ cm}^4$ $* i_y = 5.03 \text{ cm}$ $kc = 1.00$
○ R1G12 中央 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{bx} = 1450.00 \text{ cm}$
 $L_{by} = 1450.00 \text{ cm}$
 $(M_2 / M_1) = 1.000$

部材種別 = 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b : M_{FTB} = M_p - e \lambda b \geq \lambda b > p \lambda b : (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b] / (1.29 - p \lambda b)) \times M_p$ $\lambda b > e \lambda b : M_p / \lambda b^2 =$

$M_e = C \times Z \times \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$ $\rightarrow \rightarrow C = 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 4.71 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / * i_y)^2 = 4.43 \text{ KN/cm}^2$ $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.900$ $\lambda b = \sqrt{M_p / M_e} = 1.41$

$M_{LB} = (1 - N / N_{LB}) \times Z \times \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z \times \min \{ 291.25, 269.85 \} =$ ←← FA、FBは省略
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 2014.79 \text{ KN}$

※、上記結果により $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 3.950$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b$ $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.000$

$M_{pb} = 235.78 =$

使用部材 BH- 500 x 400 x 12.0 x 16.0 $Z_x = 3409.6 \text{ cm}^3$ $I_x = 85240 \text{ cm}^4$ $A = 184.16 \text{ cm}^2$
H形強軸 $Z_p = 3777.1 \text{ cm}^3$ $I_y = 17073 \text{ cm}^4$ $k_c = 1.00$
○ R1G13 端部 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{bx} = 1000.00 \text{ cm}$
 $L_{by} = 500.00 \text{ cm}$
 $(M_2 / M_1) = 0.000$

部材種別 - FC 鉛直軸力 - 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$ 976.39 KNm

$M_{FTB} = p \lambda b \geq \lambda b : M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b : (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b] / (1.29 - p \lambda b)) \times M_p$ $\lambda b > e \lambda b : M_p / \lambda b^2 =$ 976.39 KNm

$M_e = C \times Z_x \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$ 11910.83 KNm

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$ $\rightarrow C = 1.75$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 34.94 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 196.54 \text{ KN/cm}^2$ $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.600$ $\lambda b = \sqrt{M_p / M_e} = 0.29$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \min \{ 242.49, 287.69 \} =$ 826.78 KNm

$N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) =$ 2367.88 KN

※、上記結果により $M_b =$ 826.78 KNm

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 0.580$

$N_y = F \times A =$ 4760.54 KN

$N_{Ex} = \pi^2 \times E \times I / (k c^2 \times L_{bx}^2) =$ 17666.89 KN

$N_{Ey} = \pi^2 \times E \times I / (k c^2 \times L_{by}^2) =$ 14154.65 KN

※、 $N_c =$ 4006.46 KN

$N / N_y \leq 0.15 : M_{pb} = M_b$ $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.000$

$M_{pb} = 826.78 =$ 826.78 KNm

使用部材 H- 496 x 199 x 9.0 x 14.0 $Z_x = 1650.0 \text{ cm}^3$ $I_x = 40800 \text{ cm}^4$ $A = 99.29 \text{ cm}^2$
H形強軸 $Z_p = 1870.0 \text{ cm}^3$ $I_y = 1840 \text{ cm}^4$ $k_c = 1.00$
○ RIG13 中央 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{bx} = 1000.00 \text{ cm}$
 $L_{by} = 500.00 \text{ cm}$
 $(M_2 / M_1) = 0.000$

部材種別 = 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b : M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b : (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b] / (1.29 - p \lambda b)) \times M_p$
 $\lambda b > e \lambda b : M_p / \lambda b^2 =$

$M_e = C \times Z_x \times \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$ →→ $C = 1.75$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 15.33 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 38.94 \text{ KN/cm}^2$ $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.600$ $\lambda b = \sqrt{M_p / M_e} = 0.63$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \times \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \times \min \{ 287.31, 274.51 \} =$ ←← FA、FBは省略
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 1744.14 \text{ KN}$

※、上記結果により $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 1.297$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b$ $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.000$

$M_{pb} = 474.29 =$

使用部材 H- 396 x 199 x 7.0 x 11.0 $Z_x = 999.0 \text{ cm}^3$ $I_x = 19800 \text{ cm}^4$ $A = 71.41 \text{ cm}^2$
H形強軸 $Z_p = 1110.0 \text{ cm}^3$ $I_y = 1450 \text{ cm}^4$ $k_c = 1.00$
○ R2G1 端部、中央 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{bx} = 1000.00 \text{ cm}$
 $L_{by} = 1000.00 \text{ cm}$
 $(M_2 / M_1) = 1.000$

部材種別 = 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b: M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b: (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b] / (1.29 - p \lambda b)) \times M_p$ $\lambda b > e \lambda b: M_p / \lambda b^2 =$

$M_e = C \times Z_x \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$ $\rightarrow C = 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 7.55 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 10.08 \text{ KN/cm}^2$ $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.900$ $\lambda b = \sqrt{M_p / M_e} = 1.00$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \min \{ 271.20, 273.06 \} =$ ←← FA、FBは省略
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 1071.24 \text{ KN}$

※、上記結果により $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 2.478$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b$ $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.000$

$M_{pb} = 258.7 =$

使用部材 H- 600 x 200 x 11.0 x 17.0 $Z_x = 2520.0 \text{ cm}^3$ $I_x = 75600 \text{ cm}^4$ $A = 131.70 \text{ cm}^2$
H形強軸 $Z_p = 2900.0 \text{ cm}^3$ $I_y = 2270 \text{ cm}^4$ $* i_y = 5.09 \text{ cm}$ $kc = 1.00$
○ R2G2 端部、中央 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{bx} = 1000.00 \text{ cm}$
 $L_{by} = 1000.00 \text{ cm}$
 $(M_2 / M_1) = 1.000$

部材種別 = 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b : M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b : (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b] / (1.29 - p \lambda b)) \times M_p$
 $\lambda b > e \lambda b : M_p / \lambda b^2 =$

$M_e = C \times Z_x \times \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$ →→ $C = 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 7.74 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / * i_y)^2 = 9.55 \text{ KN/cm}^2$ $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.900$ $\lambda b = \sqrt{M_p / M_e} = 1.03$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \times \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \times \min \{ 297.49, 275.06 \} =$ ←← FA、FBは省略
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 2527.00 \text{ KN}$

※、上記結果により $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 2.690$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b$ $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.000$

$M_{pb} = 652.77 =$

使用部材 H- 600 x 200 x 11.0 x 17.0 $Z_x = 2520.0 \text{ cm}^3$ $I_x = 75600 \text{ cm}^4$ $A = 131.70 \text{ cm}^2$
H形強軸 $Z_p = 2900.0 \text{ cm}^3$ $I_y = 2270 \text{ cm}^4$ $k_c = 1.00$
○ R2G2 端部 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{bx} = 1400.00 \text{ cm}$
 $L_{by} = 467.00 \text{ cm}$
 $(M_2 / M_1) = -0.333$

部材種別 - FA 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$ 749.65 KNm

$M_{FTB} = p \lambda b \geq \lambda b: M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b: (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b]) / (1.29 - p \lambda b) \times M_p$ $\lambda b > e \lambda b: M_p / \lambda b^2 =$ 686.72 KNm

$M_e = C \times Z_x \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$ 1690.79 KNm

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$ $\rightarrow C = 1.43$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 16.56 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 43.77 \text{ KN/cm}^2$ $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.500$ $\lambda b = \sqrt{M_p / M_e} = 0.67$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \min \{ 297.49, 275.06 \} =$ ---- $\leftarrow \leftarrow$ FA、FBは省略
 $N_{LB} = N_y / (0.60 + 1.60 \times F_y / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 2527.00 \text{ KN}$

※、上記結果により $M_b =$ 686.72 KNm

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 1.256$

$N_y = F \times A =$ 3404.45 KN

$N_{Ex} = \pi^2 \times E \times I / (k^2 \times L_{bx}^2) =$ 7994.38 KN

$N_{Ey} = \pi^2 \times E \times I / (k^2 \times L_{by}^2) =$ 2157.30 KN

※、 $N_c =$ 1790.56 KN

$N / N_y \leq 0.15 : M_{pb} = M_b$ $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.000$

$M_{pb} = 686.72 =$ 686.72 KNm

使用部材 H- 600 x 200 x 11.0 x 17.0 $Z_x = 2520.0 \text{ cm}^3$ $I_x = 75600 \text{ cm}^4$ $A = 131.70 \text{ cm}^2$
H形強軸 $Z_p = 2900.0 \text{ cm}^3$ $I_y = 2270 \text{ cm}^4$ $* i_y = 5.09 \text{ cm}$ $k_c = 1.00$
○ R2G2 中央 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{bx} = 1400.00 \text{ cm}$
 $L_{by} = 467.00 \text{ cm}$
 $(M_2 / M_1) = 1.000$

部材種別 = 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b : M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b : (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b] / (1.29 - p \lambda b)) \times M_p$
 $\lambda b > e \lambda b : M_p / \lambda b^2 =$

$M_e = C \times Z_x \times \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$ →→ $C = 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 16.56 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / * i_y)^2 = 43.77 \text{ KN/cm}^2$ $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.900$ $\lambda b = \sqrt{M_p / M_e} = 0.53$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \times \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \times \min \{ 297.49, 275.06 \} =$ ←← FA、FBは省略
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 2527.00 \text{ KN}$

※、上記結果により $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 1.256$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b$ $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.000$

$M_{pb} = 749.65 =$

使用部材 H- 692 x 300 x 13.0 x 20.0 $Z_x = 4870.0 \text{ cm}^3$ $I_x = 168000 \text{ cm}^4$ $A = 207.50 \text{ cm}^2$
H形強軸 $Z_p = 5500.0 \text{ cm}^3$ $I_y = 9020 \text{ cm}^4$ $k_c = 1.00$
○ R2G3 端部、中央 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{bx} = 1000.00 \text{ cm}$
 $L_{by} = 500.00 \text{ cm}$
 $(M_2 / M_1) = 0.000$

部材種別 = 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b: M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b: (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b]) / (1.29 - p \lambda b) \times M_p$
 $\lambda b > e \lambda b: M_p / \lambda b^2 =$

$M_e = C \times Z_x \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$ →→ $C = 1.75$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 23.67 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 89.90 \text{ KN/cm}^2$ $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.600$ $\lambda b = \sqrt{M_p / M_e} = 0.42$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \min \{ 284.05, 276.38 \} =$ ←← FA、FBは省略
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 3627.96 \text{ KN}$

※、上記結果により $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 0.847$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b$ $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.000$

$M_{pb} = 1421.75 =$