

使用部材 H- 692 x 300 x 13.0 x 20.0 $Z_x = 4870.0 \text{ cm}^3$ $I_x = 168000 \text{ cm}^4$ $A = 207.50 \text{ cm}^2$
 H形強軸 $I_y = 9020 \text{ cm}^4$
 $Z_p = 5500.0 \text{ cm}^3$ * $i_y = 7.81 \text{ cm}$ $k_c = 1.00$
 ○ R2G3 端部 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$
 Y5-6
 強度割増 = 1.1 倍 $L_{bx} = 1000.00 \text{ cm}$
 $L_{by} = 250.00 \text{ cm}$
 $(M_2 / M_1) = -0.500$

部材種別 = 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b: M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b: (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b] / (1.29 - p \lambda b)) \times M_p$
 $\lambda b > e \lambda b: M_p / \lambda b^2 =$

$M_e = C \times Z_x \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$ →→ $C = 1.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 47.34 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 359.60 \text{ KN/cm}^2$ $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.450$ $\lambda b = \sqrt{M_p / M_e} = 0.25$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \min \{ 284.05, 276.38 \} =$ ←← FA、FBは省略
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 3627.96 \text{ KN}$

※、上記結果により $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 0.423$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b$ $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.000$

$M_{pb} = 1421.75 =$

使用部材 H- 692 x 300 x 13.0 x 20.0 $Z_x = 4870.0 \text{ cm}^3$ $I_x = 168000 \text{ cm}^4$ $A = 207.50 \text{ cm}^2$
 H形強軸 $Z_p = 5500.0 \text{ cm}^3$ $I_y = 9020 \text{ cm}^4$ $k_c = 1.00$
 $* i_y = 7.81 \text{ cm}$
 ○ R2G3 中央 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$
 Y5-6
 強度割増 = 1.1 倍 $L_{bx} = 1000.00 \text{ cm}$
 $L_{by} = 250.00 \text{ cm}$
 $(M_2 / M_1) = 0.000$

部材種別 = 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b: M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b: (1 - 0.4 \times [(\sqrt{M_p/M_e}) - p \lambda b] / (1.29 - p \lambda b)) \times M_p$
 $\lambda b > e \lambda b: M_p / \lambda b^2 =$

$M_e = C \times Z_x \times \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$ →→ $C = 1.75$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 47.34 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / * i_y)^2 = 359.60 \text{ KN/cm}^2$ $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.600$ $\lambda b = \sqrt{M_p/M_e} = 0.21$

$M_{LB} = (1 - N / N_LB) \times Z_x \times \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \times \min \{ 284.05, 276.38 \} =$ ←← FA、FBは省略
 $N_{LB} = N_y / (0.60 + 1.60 \times F_yf / E \times (b / t_f)^2 + 0.15 \times F_yw / E \times (d / t_w)^2) = 3627.96 \text{ KN}$

※、上記結果により $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 0.423$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b$ $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.000$

$M_{pb} = 1421.75 =$

使用部材 H- 692 x 300 x 13.0 x 20.0 $Z_x = 4870.0 \text{ cm}^3$ $I_x = 168000 \text{ cm}^4$ $A = 207.50 \text{ cm}^2$
 $I_y = 9020 \text{ cm}^4$
 H形強軸 $Z_p = 5500.0 \text{ cm}^3$ * $i_y = 7.81 \text{ cm}$ $k_c = 1.00$
 ○ R2G3 端部、中央 Y4-5 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$
 強度割増 = 1.1 倍 $L_{bx} = 500.00 \text{ cm}$
 $L_{by} = 500.00 \text{ cm}$
 $(M_2 / M_1) = 1.000$

部材種別 = FA 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$ 1421.75 KNm

$M_{FTB} = p \lambda b \geq \lambda b : M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b : (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b]) /$
 $(1.29 - p \lambda b)] \times M_p \quad \lambda b > e \lambda b : M_p / \lambda b^2 =$ 1421.75 KNm

$M_e = C \times Z_x \times \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$ 10412.87 KNm

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30 \quad \rightarrow \rightarrow C = 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 23.67 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 89.90 \text{ KN/cm}^2 \quad e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.900 \quad \lambda b = \sqrt{M_p / M_e} = 0.37$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \times \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \times \min \{ 284.05, 276.38 \} =$ ----- ←← FA、FBは省略
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 3627.96 \text{ KN}$

※、上記結果により $M_b =$ 1421.75 KNm

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 0.847$

$N_y = F \times A =$ 5363.88 KN

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) =$ 139279.86 KN

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) =$ 7478.00 KN

※、 $N_c =$ 5276.19 KN

$N / N_y \leq 0.15 : M_{pb} = M_b \quad N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c) \quad N / N_y = 0.000$

$M_{pb} = 1421.75 =$ 1421.75 KNm

使用部材 H- 496 x 199 x 9.0 x 14.0 $Z_x = 1650.0 \text{ cm}^3$ $I_x = 40800 \text{ cm}^4$ $A = 99.29 \text{ cm}^2$
H形強軸 $Z_p = 1870.0 \text{ cm}^3$ $I_y = 1840 \text{ cm}^4$ $k_c = 1.00$
○ R2G4 端部、中央 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{bx} = 1000.00 \text{ cm}$
 $L_{by} = 1000.00 \text{ cm}$
 $(M_2 / M_1) = 1.000$

部材種別 - FA 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$ 483.40 KNm

$M_{FTB} = p \lambda b \geq \lambda b : M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b : (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b] / (1.29 - p \lambda b)) \times M_p$ $\lambda b > e \lambda b : M_p / \lambda b^2 =$ 426.94 KNm

$M_e = C \times Z_x \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$ 470.26 KNm

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$ $\rightarrow \rightarrow C = 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 7.67 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 9.73 \text{ KN/cm}^2$ $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.900$ $\lambda b = \sqrt{M_p / M_e} = 1.01$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \min \{ 287.31, 274.51 \} =$ ---- $\leftarrow \leftarrow$ FA、FBは省略
 $N_{LB} = N_y / (0.60 + 1.60 \times F_y f / E \times (b / t_f)^2 + 0.15 \times F_y w / E \times (d / t_w)^2) = 1744.14 \text{ KN}$

※、上記結果により $M_b =$ 426.94 KNm

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 2.594$

$N_y = F \times A =$ 2566.65 KN

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) =$ 8456.28 KN

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) =$ 381.36 KN

※、 $N_c =$ 316.53 KN

$N / N_y \leq 0.15 : M_{pb} = M_b$ $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.000$

$M_{pb} = 426.94 =$ 426.94 KNm

使用部材 H- 496 x 199 x 9.0 x 14.0 $Z_x = 1650.0 \text{ cm}^3$ $I_x = 40800 \text{ cm}^4$ $A = 99.29 \text{ cm}^2$
H形強軸 $Z_p = 1870.0 \text{ cm}^3$ $I_y = 1840 \text{ cm}^4$ $k_c = 1.00$
○ R2G4 端部 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{bx} = 1200.00 \text{ cm}$
 $L_{by} = 1200.00 \text{ cm}$
 $(M_2 / M_1) = 1.000$

部材種別 = FA 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$ 483.40 KNm

$M_{FTB} = p \lambda b \geq \lambda b : M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b : (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b] / (1.29 - p \lambda b)) \times M_p$ $\lambda b > e \lambda b : M_p / \lambda b^2 =$ 349.43 KNm

$M_e = C \times Z_x \times \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$ 353.00 KNm

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$ →→ $C = 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 6.39 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 6.76 \text{ KN/cm}^2$ $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.900$ $\lambda b = \sqrt{M_p / M_e} = 1.17$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \times \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \times \min \{ 287.31, 274.51 \} =$ ---- ←← FA、FBは省略
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 1744.14 \text{ KN}$

※、上記結果により $M_b =$ 349.43 KNm

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 3.113$

$N_y = F \times A =$ 2566.65 KN

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) =$ 5872.41 KN

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) =$ 264.83 KN

※、 $N_c =$ 219.81 KN

$N / N_y \leq 0.15 : M_{pb} = M_b$ $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.000$

$M_{pb} = 349.43 =$ 349.43 KNm

使用部材 H- 496 x 199 x 9.0 x 14.0 $Z_x = 1650.0 \text{ cm}^3$ $I_x = 40800 \text{ cm}^4$ $A = 99.29 \text{ cm}^2$
H形強軸 $I_y = 1840 \text{ cm}^4$
 $Z_p = 1870.0 \text{ cm}^3$ * $i_y = 5.14 \text{ cm}$ $k_c = 1.00$
○ R2G4 中央 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{bx} = 1200.00 \text{ cm}$
 $L_{by} = 1200.00 \text{ cm}$
 $(M_2 / M_1) = 1.000$

部材種別 = 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b : M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b : (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b] / (1.29 - p \lambda b)) \times M_p$
 $\lambda b > e \lambda b : M_p / \lambda b^2 =$

$M_e = C \times Z_x \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$ →→ $C = 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 6.39 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 6.76 \text{ KN/cm}^2$ $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.900$ $\lambda b = \sqrt{M_p / M_e} = 1.17$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \min \{ 287.31, 274.51 \} =$ ←← FA、FBは省略
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 1744.14 \text{ KN}$

※、上記結果により $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 3.113$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b$ $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.000$

$M_{pb} = 349.43 =$

使用部材 H- 496 x 199 x 9.0 x 14.0 $Z_x = 1650.0 \text{ cm}^3$ $I_x = 40800 \text{ cm}^4$ $A = 99.29 \text{ cm}^2$
H形強軸 $Z_p = 1870.0 \text{ cm}^3$ $I_y = 1840 \text{ cm}^4$ $k_c = 1.00$
○ R2G4 端部 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{bx} = 1400.00 \text{ cm}$
 $L_{by} = 1400.00 \text{ cm}$
 $(M_2 / M_1) = 1.000$

部材種別 = 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b : M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b : (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b] / (1.29 - p \lambda b)) \times M_p$ $\lambda b > e \lambda b : M_p / \lambda b^2 =$

$M_e = C \times Z_x \times \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$ →→ $C = 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 5.48 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 4.97 \text{ KN/cm}^2$ $c \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.900$ $\lambda b = \sqrt{M_p / M_e} = 1.31$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \times \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \times \min \{ 287.31, 274.51 \} =$ ←← FA、FBは省略
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 1744.14 \text{ KN}$

※、上記結果により $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 3.632$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b$ $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.000$

$M_{pb} = 213.76 =$

使用部材 H- 496 x 199 x 9.0 x 14.0 $Z_x = 1650.0 \text{ cm}^3$ $I_x = 40800 \text{ cm}^4$ $A = 99.29 \text{ cm}^2$
H形強軸 $I_y = 1840 \text{ cm}^4$
 $Z_p = 1870.0 \text{ cm}^3$ * $i_y = 5.14 \text{ cm}$ $k_c = 1.00$
○ R2G4 中央 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{bx} = 1400.00 \text{ cm}$
 $L_{by} = 1400.00 \text{ cm}$
 $(M_2 / M_1) = 1.000$

部材種別 = 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b : M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b : (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b] / (1.29 - p \lambda b)) \times M_p$ $\lambda b > e \lambda b : M_p / \lambda b^2 =$

$M_e = C \times Z_x \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$ →→ $C = 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 5.48 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 4.97 \text{ KN/cm}^2$ $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.900$ $\lambda b = \sqrt{M_p / M_e} = 1.31$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \min \{ 287.31, 274.51 \} =$ ←← FA、FBは省略
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 1744.14 \text{ KN}$

※、上記結果により $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 3.632$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b$ $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.000$

$M_{pb} = 213.76 =$

使用部材 H- 900 x 300 x 16.0 x 28.0 $Z_x = 8990.0 \text{ cm}^3$ $I_x = 404000 \text{ cm}^4$ $A = 305.80 \text{ cm}^2$
H形強軸 $Z_p = 10300.0 \text{ cm}^3$ $I_y = 12600 \text{ cm}^4$ $kc = 1.00$
○ R2G5 端部 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{bx} = 1000.00 \text{ cm}$
 $L_{by} = 250.00 \text{ cm}$
 $(M_2 / M_1) = -0.500$

部材種別 = 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b : M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b : (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b] / (1.29 - p \lambda b)) \times M_p$ $\lambda b > e \lambda b : M_p / \lambda b^2 =$

$M_e = C \times Z_x \times \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$ →→ $C = 1.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 50.96 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 354.10 \text{ KN/cm}^2$ $c \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.450$ $\lambda b = \sqrt{M_p / M_e} = 0.25$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \times \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \times \min \{ 301.86, 273.75 \} =$ ←← FA、FBは省略
 $N_{LB} = N_y / (0.60 + 1.60 \times F_y f / E \times (b / t_f)^2 + 0.15 \times F_y w / E \times (d / t_w)^2) = 5913.99 \text{ KN}$

※、上記結果により $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 0.435$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b$ $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.000$

$M_{pb} = 2662.55 =$

使用部材 H- 900 x 300 x 16.0 x 28.0 $Z_x = 8990.0 \text{ cm}^3$ $I_x = 404000 \text{ cm}^4$ $A = 305.80 \text{ cm}^2$
H形強軸 $Z_p = 10300.0 \text{ cm}^3$ $I_y = 12600 \text{ cm}^4$ $k_c = 1.00$
○ R2G5 中央 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{bx} = 1000.00 \text{ cm}$
 $L_{by} = 250.00 \text{ cm}$
 $(M_2 / M_1) = 0.000$

部材種別 = 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b : M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b : (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b]) / (1.29 - p \lambda b) \times M_p$
 $\lambda b > e \lambda b : M_p / \lambda b^2 =$

$M_e = C \times Z_x \times \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$ →→ $C = 1.75$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 50.96 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 354.10 \text{ KN/cm}^2$ $c \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.600$ $\lambda b = \sqrt{M_p / M_e} = 0.22$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \times \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \times \min \{ 301.86, 273.75 \} =$ ←← FA、FBは省略
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 5913.99 \text{ KN}$

※、上記結果により $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 0.435$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b$ $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.000$

$M_{pb} = 2662.55 =$

使用部材 H- 900 x 300 x 16.0 x 28.0 $Z_x = 8990.0 \text{ cm}^3$ $I_x = 404000 \text{ cm}^4$ $A = 305.80 \text{ cm}^2$
H形強軸 $Z_p = 10300.0 \text{ cm}^3$ $I_y = 12600 \text{ cm}^4$ $k_c = 1.00$
○ R2G5 端部、中央 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{bx} = 500.00 \text{ cm}$
 $L_{by} = 500.00 \text{ cm}$
 $(M_2 / M_1) = 1.000$

部材種別 = 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b : M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b : (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b] / (1.29 - p \lambda b)) \times M_p$ $\lambda b > e \lambda b : M_p / \lambda b^2 =$

$M_e = C \times Z_x \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$ →→ $C = 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 25.48 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 88.52 \text{ KN/cm}^2$ $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.900$ $\lambda b = \sqrt{M_p / M_e} = 0.37$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \min \{ 301.86, 273.75 \} =$ ←← FA、FBは省略
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 5913.99 \text{ KN}$

※、上記結果により $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 0.870$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b$ $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.000$

$M_{pb} = 2662.55 =$

使用部材 H- 606 x 201 x 12.0 x 20.0 $Z_x = 2910.0 \text{ cm}^3$ $I_x = 88300 \text{ cm}^4$ $A = 149.80 \text{ cm}^2$
H形強軸 $I_y = 2720 \text{ cm}^4$
 $Z_p = 3360.0 \text{ cm}^3$ * $i_y = 5.17 \text{ cm}$ $k_c = 1.00$
○ R2G6 端部 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{bx} = 1400.00 \text{ cm}$
 $L_{by} = 467.00 \text{ cm}$
 $(M_2 / M_1) = -0.333$

部材種別 = 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b: M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b: (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b]) / (1.29 - p \lambda b) \times M_p$ $\lambda b > e \lambda b: M_p / \lambda b^2 =$

$M_e = C \times Z_x \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$ $\rightarrow C = 1.43$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 19.39 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 45.16 \text{ KN/cm}^2$ $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.500$ $\lambda b = \sqrt{M_p / M_e} = 0.65$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \min \{ 304.62, 279.41 \} =$ ←← FA、FBは省略
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 3203.13 \text{ KN}$

※、上記結果により $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 1.224$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b$ $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.000$

$M_{pb} = 802.25 =$

使用部材 H- 606 x 201 x 12.0 x 20.0 $Z_x = 2910.0 \text{ cm}^3$ $I_x = 88300 \text{ cm}^4$ $A = 149.80 \text{ cm}^2$
H形強軸 $Z_p = 3360.0 \text{ cm}^3$ $I_y = 2720 \text{ cm}^4$ $k_c = 1.00$
○ R2G6 中央 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{bx} = 1400.00 \text{ cm}$
 $L_{by} = 467.00 \text{ cm}$
 $(M_2 / M_1) = 1.000$

部材種別 = 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b: M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b: (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b] / (1.29 - P \lambda b)) \times M_p$ $\lambda b > e \lambda b: M_p / \lambda b^2 =$

$M_e = C \times Z_x \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30 \rightarrow C = 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 19.39 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 45.16 \text{ KN/cm}^2$ $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.900$ $\lambda b = \sqrt{M_p / M_e} = 0.51$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \min \{ 304.62, 279.41 \} =$ ←← FA、FBは省略
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 3203.13 \text{ KN}$

※、上記結果により $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 1.224$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b$ $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.000$

$M_{pb} = 868.56 =$

使用部材 H- 588 x 300 x 12.0 x 20.0 $Z_x = 3890.0 \text{ cm}^3$ $I_x = 114000 \text{ cm}^4$ $A = 187.20 \text{ cm}^2$
H形強軸 $Z_p = 4350.0 \text{ cm}^3$ $I_y = 9010 \text{ cm}^4$ $k_c = 1.00$
○ R2G7 端部、中央 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{bx} = 1200.00 \text{ cm}$
 $L_{by} = 1200.00 \text{ cm}$
 $(M_2 / M_1) = 1.000$

部材種別 = 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b: M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b: (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b]) / (1.29 - p \lambda b) \times M_p$
 $\lambda b > e \lambda b: M_p / \lambda b^2 =$

$M_e = C \times Z_x \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30 \rightarrow C = 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 11.61 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 16.42 \text{ KN/cm}^2$ $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.900$ $\lambda b = \sqrt{M_p / M_e} = 0.79$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \min \{ 284.05, 280.93 \} =$ ←← FA、FBは省略
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 3442.05 \text{ KN}$

※、上記結果により $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 1.932$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b$ $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.000$

$M_{pb} = 1124.48 =$

使用部材 H- 596 x 199 x 10.0 x 15.0 $Z_x = 2240.0 \text{ cm}^3$ $I_x = 66600 \text{ cm}^4$ $A = 117.80 \text{ cm}^2$
H形強軸 $Z_p = 2580.0 \text{ cm}^3$ * $i_y = 5.03 \text{ cm}$ $k_c = 1.00$
○ R2G8 端部 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{bx} = 1400.00 \text{ cm}$
 $L_{by} = 467.00 \text{ cm}$
 $(M_2 / M_1) = -0.333$

部材種別 = 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b : M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b : (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b] / (1.29 - p \lambda b)) \times M_p$ $\lambda b > e \lambda b : M_p / \lambda b^2 =$

$M_e = C \times Z_x \times \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$ →→ $C = 1.43$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 14.64 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 42.75 \text{ KN/cm}^2$ $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.500$ $\lambda b = \sqrt{M_p / M_e} = 0.68$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \times \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \times \min \{ 291.25, 269.85 \} =$ ←← FA, FBは省略
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 2014.79 \text{ KN}$

※、上記結果により $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 1.272$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I_x / (k_c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I_y / (k_c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b$ $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.000$

$M_{pb} = 606.86 =$

使用部材 H- 596 x 199 x 10.0 x 15.0 $Z_x = 2240.0 \text{ cm}^3$ $I_x = 66600 \text{ cm}^4$ $A = 117.80 \text{ cm}^2$
H形強軸 $Z_p = 2580.0 \text{ cm}^3$ $I_y = 1980 \text{ cm}^4$ $k_c = 1.00$
○ R2G8 中央 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{bx} = 1400.00 \text{ cm}$
 $L_{by} = 467.00 \text{ cm}$
 $(M_2 / M_1) = 1.000$

部材種別 = 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b: M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b: (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b]) / (1.29 - p \lambda b) \times M_p$
 $\lambda b > e \lambda b: M_p / \lambda b^2 =$

$M_e = C \times Z_x \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$ →→ $C = 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 14.64 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 42.75 \text{ KN/cm}^2$ $c \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.900$ $\lambda b = \sqrt{M_p / M_e} = 0.54$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \min \{ 291.25, 269.85 \} =$ ←← FA、FBは省略
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 2014.79 \text{ KN}$

※、上記結果により $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 1.272$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b$ $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.000$

$M_{pb} = 666.93 =$

使用部材 H- 596 x 199 x 10.0 x 15.0 $Z_x = 2240.0 \text{ cm}^3$ $I_x = 66600 \text{ cm}^4$ $A = 117.80 \text{ cm}^2$
H形強軸 $I_y = 1980 \text{ cm}^4$
 $Z_p = 2580.0 \text{ cm}^3$ * $i_y = 5.03 \text{ cm}$ $k_c = 1.00$
○ R2G8 端部 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{bx} = 1200.00 \text{ cm}$
 $L_{by} = 1200.00 \text{ cm}$
 $(M_2 / M_1) = 1.000$

部材種別 - FA 鉛直軸力 - 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$ 666.93 KNm

$M_{FTB} = p \lambda b \geq \lambda b : M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b : (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b] / (1.29 - p \lambda b)) \times M_p$ $\lambda b > e \lambda b : M_p / \lambda b^2 =$ 444.49 KNm

$M_e = C \times Z_x \times \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$ 444.29 KNm

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$ $\rightarrow \rightarrow C = 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 5.70 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 6.47 \text{ KN/cm}^2$ $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.900$ $\lambda b = \sqrt{M_p / M_e} = 1.23$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \times \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \times \min \{ 291.25, 269.85 \} =$ ---- ←← FA、FBは省略
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 2014.79 \text{ KN}$

※、上記結果により $M_b =$ 444.49 KNm

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 3.269$

$N_y = F \times A =$ 3045.13 KN

$N_{Ex} = \pi^2 \times E \times I / (k c^2 \times L_{bx}^2) =$ 9585.85 KN

$N_{Ey} = \pi^2 \times E \times I / (k c^2 \times L_{by}^2) =$ 284.98 KN

※、 $N_c =$ 236.54 KN

$N / N_y \leq 0.15 : M_{pb} = M_b$ $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.000$

$M_{pb} = 444.49 =$ 444.49 KNm

使用部材 H- 596 x 199 x 10.0 x 15.0 $Z_x = 2240.0 \text{ cm}^3$ $I_x = 66600 \text{ cm}^4$ $A = 117.80 \text{ cm}^2$
H形強軸 $Z_p = 2580.0 \text{ cm}^3$ $I_y = 1980 \text{ cm}^4$ $k_c = 1.00$
○ R2G8 中央 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{bx} = 1200.00 \text{ cm}$
 $L_{by} = 1200.00 \text{ cm}$
 $(M_2 / M_1) = 1.000$

部材種別 = 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b : M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b : (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b] / (1.29 - p \lambda b)) \times M_p$
 $\lambda b > e \lambda b : M_p / \lambda b^2 =$

$M_e = C \times Z_x \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$ $\rightarrow \rightarrow C = 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 5.70 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 6.47 \text{ KN/cm}^2$ $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.900$ $\lambda b = \sqrt{M_p / M_e} = 1.23$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \min \{ 291.25, 269.85 \} =$ ← FA、FBは省略
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 2014.79 \text{ KN}$

※、上記結果により $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 3.269$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b$ $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.000$

$M_{pb} = 444.49 =$

使用部材 H- 606 x 201 x 12.0 x 20.0 $Z_x = 2910.0 \text{ cm}^3$ $I_x = 88300 \text{ cm}^4$ $A = 149.80 \text{ cm}^2$
H形強軸 $Z_p = 3360.0 \text{ cm}^3$ $I_y = 2720 \text{ cm}^4$ $k_c = 1.00$
○ R2G9 端部 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{bx} = 1400.00 \text{ cm}$
 $L_{by} = 1400.00 \text{ cm}$
 $(M_2 / M_1) = 1.000$

部材種別 = 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b : M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b : (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b] / (1.29 - p \lambda b)) \times M_p$ $\lambda b > e \lambda b : M_p / \lambda b^2 =$

$M_e = C \times Z_x \times \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$ →→ $C = 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 6.47 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 5.02 \text{ KN/cm}^2$ $c \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.900$ $\lambda b = \sqrt{M_p / M_e} = 1.26$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \times \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \times \min \{ 304.62, 279.41 \} =$ ←← FA、FBは省略
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 3203.13 \text{ KN}$

※、上記結果により $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 3.669$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b$ $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.000$

$M_{pb} = 548.98 =$

使用部材 H- 596 x 199 x 10.0 x 15.0 $Z_x = 2240.0 \text{ cm}^3$ $I_x = 66600 \text{ cm}^4$ $A = 117.80 \text{ cm}^2$
H形強軸 $Z_p = 2580.0 \text{ cm}^3$ $I_y = 1980 \text{ cm}^4$ $k_c = 1.00$
○ R2G9 中央 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{bx} = 1400.00 \text{ cm}$
 $L_{by} = 1400.00 \text{ cm}$
 $(M_2 / M_1) = 1.000$

部材種別 = 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b : M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b : (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b] / (1.29 - p \lambda b)) \times M_p$ $\lambda b > e \lambda b : M_p / \lambda b^2 =$

$M_e = C \times Z_x \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$ →→ $C = 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 4.88 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 4.76 \text{ KN/cm}^2$ $e \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.900$ $\lambda b = \sqrt{M_p / M_e} = 1.38$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \min \{ 291.25, 269.85 \} =$ ←← FA、FBは省略
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 2014.79 \text{ KN}$

※、上記結果により $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 3.814$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b$ $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.000$

$M_{pb} = 254.86 =$

使用部材 H- 606 x 201 x 12.0 x 20.0 $Z_x = 2910.0 \text{ cm}^3$ $I_x = 88300 \text{ cm}^4$ $A = 149.80 \text{ cm}^2$
H形強軸 $Z_p = 3360.0 \text{ cm}^3$ $I_y = 2720 \text{ cm}^4$ $k_c = 1.00$
○ R2G9 端部、中央 $F = 235 \text{ N/mm}^2$ $F_u = 400 \text{ N/mm}^2$

強度割増 = 1.1 倍 $L_{bx} = 1200.00 \text{ cm}$
 $L_{by} = 1200.00 \text{ cm}$
 $(M_2 / M_1) = 1.000$

部材種別 = 鉛直軸力 = 0.00 KN

$M_b = \min \{ M_p, M_{LB}, M_{FTB} \}$ ※、角型鋼の場合は、 M_p のみ考慮。

$M_p = F \times Z_p =$

$M_{FTB} = p \lambda b \geq \lambda b : M_{FTB} = M_p \cdot e \lambda b \geq \lambda b > p \lambda b : (1 - 0.4 \times [(\sqrt{M_p / M_e}) - p \lambda b] / (1.29 - p \lambda b)) \times M_p$ $\lambda b > e \lambda b : M_p / \lambda b^2 =$

$M_e = C \times Z_x \times \sqrt{(\sigma_{scr}^2 + \sigma_{wcr}^2)}$

$C = 1.75 + 1.05 \times (M_2 / M_1) + 0.3 \times (M_2 / M_1)^2 \leq 2.30$ →→ $C = 2.30$

$\sigma_{scr} = 0.65 \times E / (L_{by} \times h / A_f) = 7.55 \text{ KN/cm}^2$

$\sigma_{wcr} = \pi^2 \times E / (k L_{by} / i_y)^2 = 6.84 \text{ KN/cm}^2$ $c \lambda b = 1.29$

$p \lambda b = 0.6 + 0.3 \times (M_2 / M_1) = 0.900$ $\lambda b = \sqrt{M_p / M_e} = 1.13$

$M_{LB} = (1 - N / N_{LB}) \times Z_x \times \min \{ (670 - (b / t_f) \times \sqrt{F_f}) \times (F_f / 500), (5190 - (d / t_w) \times \sqrt{F_w}) \times (F_w / 4100) \}$

$= Z_x \times \min \{ 304.62, 279.41 \} =$ ←← FA、FBは省略
 $N_{LB} = N_y / (0.60 + 1.60 \times F_{yf} / E \times (b / t_f)^2 + 0.15 \times F_{yw} / E \times (d / t_w)^2) = 3203.13 \text{ KN}$

※、上記結果により $M_b =$

$N_c = \min (N_y, (1.07 - 0.44 \sqrt{N_y / N_E}) \times N_y, 0.83 \times N_E)$
 $\lambda_c = 3.145$

$N_y = F \times A =$

$N_{Ex} = \pi^2 \times E \times I / (k_c^2 \times L_{bx}^2) =$

$N_{Ey} = \pi^2 \times E \times I / (k_c^2 \times L_{by}^2) =$

※、 $N_c =$

$N / N_y \leq 0.15 : M_{pb} = M_b$ $N / N_y > 0.15 : M_{pb} = 1.18 \times M_b \times (1 - N / N_c)$ $N / N_y = 0.000$

$M_{pb} = 664.71 =$